

PATENT COOPERATION TREATY

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NOTIFICATION OF ELECTION

(PCT Rule 61.2)

From the INTERNATIONAL BUREAU

To:

Commissioner
US Department of Commerce
United States Patent and Trademark
Office, PCT
2011 South Clark Place Room
CP2/5C24
Arlington, VA 22202
ETATS-UNIS D'AMERIQUE
in its capacity as elected Office

Date of mailing (day/month/year) 14 December 2000 (14.12.00)	
International application No. PCT/EP00/03474	Applicant's or agent's file reference 990070PCT
International filing date (day/month/year) 17 April 2000 (17.04.00)	Priority date (day/month/year) 22 April 1999 (22.04.99)
Applicant WILHELM, Fritz et al	

1. The designated Office is hereby notified of its election made:

☒ in the demand filed with the International Preliminary Examining Authority on:
22 November 2000 (22.11.00)

☐ in a notice effecting later election filed with the International Bureau on:

2. The election ☒ was
☐ was not

made before the expiration of 19 months from the priority date or, where Rule 32 applies, within the time limit under Rule 32.2(b).

The International Bureau of WIPO 34, chemin des Colombettes 1211 Geneva 20, Switzerland	Authorized officer Pascal Piriou
Facsimile No.: (41-22) 740.14.35	Telephone No.: (41-22) 338.83.38

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PATENT COOPERATION TREATY

From the
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

To:

REVESZ, Veronika
Metallgesellschaft AG
c/o Lurgi AG, Abt. Patente, A-VRP
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ALLEMAGNE

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NOTIFICATION OF TRANSMITTAL OF
THE INTERNATIONAL PRELIMINARY
EXAMINATION REPORT
(PCT Rule 71.1)

Date of mailing
(day/month/year) 09.02.2001

Applicant's or agent's file reference
990070PCT

IMPORTANT NOTIFICATION

International application No.
PCT/EP00/03474

International filing date (day/month/year)
17/04/2000

Priority date (day/month/year)
22/04/1999

Applicant
LURGI ZIMMER AG et al.

1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
3. Where required by any of the elected Offices, the International Bureau will prepare an English translation of the report (but not of any annexes) and will transmit such translation to those Offices.

4. REMINDER

The applicant must enter the national phase before each elected Office by performing certain acts (filing translations and paying national fees) within 30 months from the priority date (or later in some Offices) (Article 39(1)) (see also the reminder sent by the International Bureau with Form PCT/IB/301).

Where a translation of the international application must be furnished to an elected Office, that translation must contain a translation of any annexes to the international preliminary examination report. It is the applicant's responsibility to prepare and furnish such translation directly to each elected Office concerned.

For further details on the applicable time limits and requirements of the elected Offices, see Volume II of the PCT Applicant's Guide.

Name and mailing address of the IPEA/



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PATENT COOPERATION TREATY

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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference 990070PCT	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/EP00/03474	International filing date (day/month/year) 17/04/2000	Priority date (day/month/year) 22/04/1999
International Patent Classification (IPC) or national classification and IPC C08G63/78		
Applicant LURGI ZIMMER AG et al.		
<p>1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.</p> <p>2. This REPORT consists of a total of 4 sheets, including this cover sheet.</p> <p><input type="checkbox"/> This report is also accompanied by ANNEXES, i.e. sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).</p> <p>These annexes consist of a total of sheets.</p>		
<p>3. This report contains indications relating to the following items:</p> <ul style="list-style-type: none"> I <input checked="" type="checkbox"/> Basis of the report II <input type="checkbox"/> Priority III <input type="checkbox"/> Non-establishment of opinion with regard to novelty, inventive step and industrial applicability IV <input type="checkbox"/> Lack of unity of invention V <input checked="" type="checkbox"/> Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement VI <input type="checkbox"/> Certain documents cited VII <input checked="" type="checkbox"/> Certain defects in the international application VIII <input type="checkbox"/> Certain observations on the international application 		
Date of submission of the demand 22/11/2000	Date of completion of this report 09.02.2001	
Name and mailing address of the international preliminary examining authority: <div style="display: flex; align-items: center;"> <div> European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465 </div> </div>	Authorized officer Van de Panne, V Telephone No. +49 89 2399 8405	



INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/EP00/03474

I. Basis of the report

1. This report has been drawn on the basis of *(substitute sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to the report since they do not contain amendments (Rules 70.16 and 70.17).):*

Description, pages:

1-20 as originally filed

Claims, No.:

1-19 as originally filed

2. With regard to the **language**, all the elements marked above were available or furnished to this Authority in the language in which the international application was filed, unless otherwise indicated under this item.

These elements were available or furnished to this Authority in the following language: , which is:

- ☐ the language of a translation furnished for the purposes of the international search (under Rule 23.1(b)).
- ☐ the language of publication of the international application (under Rule 48.3(b)).
- ☐ the language of a translation furnished for the purposes of international preliminary examination (under Rule 55.2 and/or 55.3).

3. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international preliminary examination was carried out on the basis of the sequence listing:

- ☐ contained in the international application in written form.
- ☐ filed together with the international application in computer readable form.
- ☐ furnished subsequently to this Authority in written form.
- ☐ furnished subsequently to this Authority in computer readable form.
- ☐ The statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.
- ☐ The statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

4. The amendments have resulted in the cancellation of:

- ☐ the description, pages:
- ☐ the claims, Nos.:
- ☐ the drawings, sheets:

5. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed (Rule 70.2(c)):

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/EP00/03474

(Any replacement sheet containing such amendments must be referred to under item 1 and annexed to this report.)

6. Additional observations, if necessary:

V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. Statement

Novelty (N)	Yes:	Claims	1-19
	No:	Claims	
Inventive step (IS)	Yes:	Claims	1-19
	No:	Claims	
Industrial applicability (IA)	Yes:	Claims	1-19
	No:	Claims	

2. Citations and explanations
see separate sheet

VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted:
see separate sheet

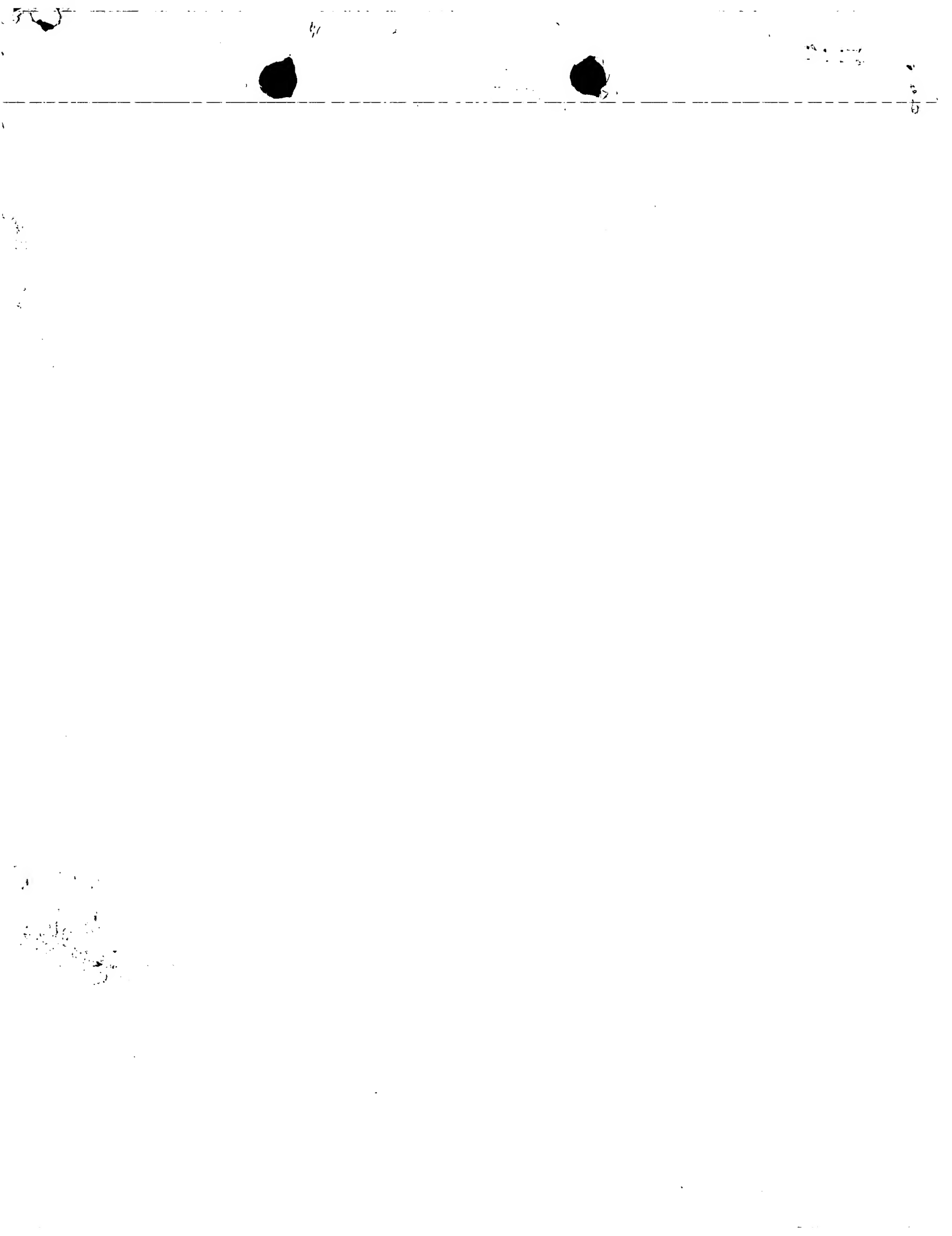


**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/EP00/03474

- I The documents cited in the search report do not disclose or suggest a process as claimed in claim 1. They do in particular not show a process in which the esterification reaction is divided in two stages with addition of the greater part of the titanium catalyst to the second stage, nor do they disclose the liquid catalyst feed as used according to claim 1.

- II The description refers on page 13 lines 1-3 and page 14 lines 26-28 to a table of results. Such a table is not included in the application as filed and cannot be added, as this would mean the introduction of new matter.



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INTERNATIONAL SEARCH REPORT

(PCT Article 18 and Rules 43 and 44)

Applicant's or agent's file reference 990070PCT	FOR FURTHER ACTION see Notification of Transmittal of International Search Report (Form PCT/ISA/220) as well as, where applicable, item 5 below.	
International application No. PCT/EP 00/ 03474	International filing date (day/month/year) 17/04/2000	(Earliest) Priority Date (day/month/year) 22/04/1999
Applicant LURGI ZIMMER AG		

This International Search Report has been prepared by this International Searching Authority and is transmitted to the applicant according to Article 18. A copy is being transmitted to the International Bureau.

This International Search Report consists of a total of 3 sheets.

☒ It is also accompanied by a copy of each prior art document cited in this report.

1. Basis of the report

- a. With regard to the **language**, the international search was carried out on the basis of the international application in the language in which it was filed, unless otherwise indicated under this item.

☐ the international search was carried out on the basis of a translation of the international application furnished to this Authority (Rule 23.1(b)).

- b. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international search was carried out on the basis of the sequence listing :

☐ contained in the international application in written form.

☐ filed together with the international application in computer readable form.

☐ furnished subsequently to this Authority in written form.

☐ furnished subsequently to this Authority in computer readable form.

☐ the statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.

☐ the statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished

2. ☐ **Certain claims were found unsearchable** (See Box I).

3. ☐ **Unity of invention is lacking** (see Box II).

4. With regard to the title,

☒ the text is approved as submitted by the applicant.

☐ the text has been established by this Authority to read as follows:

5. With regard to the abstract,

☒ the text is approved as submitted by the applicant.

☐ the text has been established, according to Rule 38.2(b), by this Authority as it appears in Box III. The applicant may, within one month from the date of mailing of this international search report, submit comments to this Authority.

6. The figure of the drawings to be published with the abstract is Figure No.

☐ as suggested by the applicant.

☐ because the applicant failed to suggest a figure.

☐ because this figure better characterizes the invention.

☒ None of the figures.



INTERNATIONAL SEARCH REPORT

International Application No

P 00/03474

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 C08G63/78 C08G63/85 C08G63/183

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 C08G

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ, CHEM ABS Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	CHEMICAL ABSTRACTS, vol. 81, no. 24, 16 December 1974 (1974-12-16) Columbus, Ohio, US; abstract no. 153134, IKEUCHI, HIROYIKI ET AL.: "Catalysts for manufacture of poly(tetramethyleneterephthalate)" XP002115471 abstract & JP 49 057092 A (TORAY INDUSTRIES) 3 June 1974 (1974-06-03)	1
A	US 5 656 716 A (SCHMIDT WOLFGANG ET AL) 12 August 1997 (1997-08-12) claims 1-11; example 16 --- -/-	1-5, 18, 19

☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

21 August 2000

Date of mailing of the international search report

30/08/2000

Name and mailing address of the ISA

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Authorized officer

Decocker, L

INTERNATIONAL SEARCH REPORT

International Application No

P 00/03474

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 466 776 A (KRAUTSTRUNK JUERGEN ET AL) 14 November 1995 (1995-11-14) claims 1-13	1-19
A	US 5 872 204 A (KUO TUNG-YING ET AL) 16 February 1999 (1999-02-16) abstract; claims 1-27	1-5, 18, 19
A	EP 0 431 977 A (DU PONT) ✓ 12 June 1991 (1991-06-12) claims 1-17	1

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

P 00/03474

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
JP 49057092	A	03-06-1974	NONE	
US 5656716	A	12-08-1997	DE 19513056 A EP 0736560 A	10-10-1996 09-10-1996
US 5466776	A	14-11-1995	DE 4419397 A DE 59505625 D EP 0685502 A ES 2129701 T	14-12-1995 20-05-1999 06-12-1995 16-06-1999
US 5872204	A	16-02-1999	NONE	
EP 0431977	A	12-06-1991	US 5015759 A CA 2031611 A JP 2894543 B JP 7053464 A JP 2031681 C JP 4108760 A JP 7039372 B KR 178061 B SG 54304 A	14-05-1991 09-06-1991 24-05-1999 28-02-1995 19-03-1996 09-04-1992 01-05-1995 15-05-1999 16-11-1998

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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁷ : C08G 63/78, 63/85, 63/183		A1	(11) International Publication Number: WO 00/64962
			(43) International Publication Date: 2 November 2000 (02.11.00)
(21) International Application Number: PCT/EP00/03474		Stephan [US/US]; 7615 Foster Creek Drive, Richmond, TX 77469 (US).	
(22) International Filing Date: 17 April 2000 (17.04.00)		(74) Agent: REVESZ, Veronika; Metallgesellschaft AG, c/o Lurgi AG, Abt. Patente, A-VRP, Lurgiallee 5, D-60295 Frankfurt am Main (DE).	
(30) Priority Data: 99107370.1 22 April 1999 (22.04.99) EP		(81) Designated States: BR, CN, JP, KR, MX, US.	
(71) Applicants (for all designated States except US): LURGI ZIMMER AG [DE/DE]; Borsigallee 1, D-60388 Frankfurt am Main (DE). SHELL INTERNATIONALE RESEARCH MAATSCHAPPIJ B.V. [NL/NL]; Carel van Bylandt Laan 30, NL-2596 HR The Hague (NL).		Published With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.	
(72) Inventors; and (75) Inventors/Applicants (for US only): WILHELM, Fritz [DE/DE]; Rendeler Strasse 79 A, D-61184 Karben (DE). SEIDEL, Eckhard [DE/DE]; Wilhelmshöher Strasse 18 D, D-60389 Frankfurt am Main (DE). REITZ, Hans [DE/DE]; Helgebornstrasse 42, D-61191 Rösbach (DE). THIELE, Ulrich [DE/DE]; Heinrich-von-Brentano-Strasse 2, D-63486 Bruchköbel (DE). MACKENSEN, Klaus [DE/DE]; Zehnmorgenstrasse 25 A, D-60433 Frankfurt am Main (DE). KELSEY, Donald, Ross [US/US]; 4706 Lake Village Drive, Fulshear, TX 77441 (US). BLACKBOURN, Robert, Lawrence [US/US]; 16410 Battlecreek Drive, Houston, TX 77095 (US). TOMASKOVIC, Robert,			

(54) Title: PROCESS OF PRODUCING POLYTRIMETHYLENE TEREPHTHALATE (PTT)

(57) Abstract

Process of producing polytrimethylene terephthalate (PTT) by esterification of terephthalic acid (TPA) with trimethylene glycol (TMG) in the presence of a catalytic titanium compound, precondensation and polycondensation. The esterification is effected in at least two stages, where in the first stage a molar ratio of TMG to TPA of 1.25 to 2.5, a content of titanium of 0 to 40 ppm, a temperature of 245 to 260 °C as well as a pressure of 1 to 3.5 bar are adjusted. In the at least one subsequent stage a content of titanium is adjusted which is higher than in the initial stage by 35 to 110 ppm. For generating the vacuum in the polycondensation and in the precondensation, there are used vapor jet pumps operated with TMG vapour.

Abt. Patente		0. NOV. 2000
	gesehen	erledigt
AMS		Dr. Que 1 0. 11. 00
DRUE		Dr. Que 1 0. 11. 00
LHG		

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EE	Estonia						

Process of producing polytrimethylene terephthalate (PTT)

Description:

This invention relates to a process of producing polytrimethylene terephthalate (PTT) with an intrinsic viscosity of at least 0.75 dl/g by esterification of terephthalic acid (TPA) with trimethylene glycol (TMG) in the presence of a catalytic titanium compound to obtain an esterification product, precondensation of the esterification product to obtain a precondensation product, and polycondensation of the precondensation product to obtain PTT.

Processes of producing PTT are known (U.S. Patents Nos. 2,456,319; 4,611,049; 5,340,909; 5,459,229; 5,599,900).

For instance, the U.S. Patent No. 4,611,049 describes the use of a protonic acid as co-catalyst for accelerating the polycondensation, where the addition of p-toluene sulfonic acid in a concentration of 50 mmol-% effects an increase of the maximum achievable intrinsic viscosity of 0.75 dl/g in a batch process catalyzed with 50 mmol-% tetrabutyl titanate to 0.90 dl/g.

The U.S. Patent No. 5,340,909 proposes to achieve an improvement of the polycondensation capacity and the color of the polytrimethylene terephthalate by using a tin

catalyst, which together with titanium can already be present in the esterification. Statements on the influence of recirculation of the vapor condensates obtained during the polycondensation on the polycondensation capacity of the reaction melt cannot be found in the U.S. Patent No. 5,340,909.

The U.S. Patent No. 5,459,229 proposes to reduce the concentration of acrolein in the vapors by adding alkalines to the condensates produced during the esterification of trimethylene glycol and terephthalic acid. The U.S. Patent No. 5,459,229 does not contain any details concerning the esterification and polycondensation.

The U.S. Patent No. 5,599,900 describes a process of producing polytrimethylene terephthalate, where in the presence of an inert stripping gas either after the transesterification or after the esterification a polytrimethylene terephthalate with a degree of polymerization of 64 is synthesized. Moreover, it is desired to also adjust higher molecular weights but this is not proven by experiment.

WO 97/23543A describes a process of producing polytrimethylene terephthalate, where it is provided to first of all produce a preproduct with an intrinsic viscosity of 0.16 dl/g by means of transesterification. This preproduct is converted to pastilles by means of dripping, which pastilles directly crystallize at crystallization temperatures up to 130°C. The actual polymer is produced subsequently by solid-phase condensation. It is disadvantageous that a high amount of trimethylene glycol and oligomers gets into the process gas and must be recovered or burnt in an expensive way.

The U.S. Patent No. 5,798,433 describes a process of producing PTT by direct esterification of terephthalic acid

with 1,3-propanediol and subsequent precondensation and polycondensation. The PTT produced contains not more than 5 ppm acrolein and 3 ppm allyl alcohol. It is obtained by esterification in the presence of 30 to 200 ppm titanium in the form of an inorganic esterification catalyst containing at least 50 mol-% TiO_2 as a precipitate, blocking the esterification catalyst after the esterification by adding 10 to 100 ppm phosphorus in the form of an oxygen containing phosphorus compound, and subsequent precondensation and polycondensation in the presence of 100 to 300 ppm antimony in the form of a usual antimony polycondensation catalyst as well as optionally adding usual color agents. The quantity of the required catalyst is very high and causes severe disadvantages in the product quality especially with regard to the thermal product stability.

From U.S. Patent No. 4,011,202 the use of glycol jet pumps is known. However, the use of TMG-jets is not yet detailed.

It is the object of the invention to create a melt phase process of producing PTT with an intrinsic viscosity between 0.75 and 1.15 dl/g and a good thermal stability, and to achieve at the same time an efficiently long service life of the filters when the polymer melt is filtered prior to processing the same to form the end products. The process may be a batch or continuous process. Additionally, the PTT process should also allow the recycling of TMG and oligomer by-products.

The foregoing objects are achieved in accordance with the invention by a process as defined in the claims.

The characteristic features of this process, which comprises the catalytic esterification of TPA with TMG, precondensation of the esterification product and

polycondensation of the precondensation product, are as follows:

- 5 - The esterification is performed in at least 2 stages, one initial stage and at least one second, subsequent stage connected to a process column.
- 10 - The catalyst used for esterification and polycondensation is a titanium compound in a stabilized liquid formulation, which is prepared from a catalytic titanium compound, an organic diacid and TMG as solvent, in such way that the liquid catalyst feed contains less than 5 wt-% titanium.
- 15 - The catalyst used for esterification in the first, initial stage can be alternatively a Ti containing liquid reaction product from TPA and TMG with a degree of esterification of at least 97%, which may be recycled from a later reaction stage and fed to the
20 initial esterification stage together with the raw materials.
- 25 - A defined quantity of the described liquid catalyst feed is introduced into the first, initial esterification stage and separately a second defined quantity of the liquid catalyst feed is added to the at least one subsequent stage of esterification.
- 30 - In the first, initial esterification stage a total molar ratio of TMG / TPA of 1.15 to 2.5, an amount of titanium of 0 to 40 ppm, which is in maximum 35% of the total amount of catalyst, a temperature of 240 to 270°C and an absolute pressure of 1 to 3,5 bar are adjusted, whereby the reaction is continued until 90 to 95% of
35 the TPA are esterified.

- In the at least one subsequent esterification stage an additional amount of titanium of 35 to 110 ppm, which is 65 to 100% of the total amount of catalyst, a temperature of 245 to 260°C and an absolute pressure of 0.7 to 1.2 bar are adjusted, whereby the reaction is continued until 97 to 99% of the TPA are esterified.
- The precondensation is performed at a temperature of 245 to 260°C under a reduced pressure in the range from 2 to 200 mbar.
- The polycondensation is carried out in the melt phase at a temperature increasing from the entry to the exit of the polycondensation reactor from 252 to 267°C and at an absolute pressure of 0.2 to 2.5 mbar.
- For generating the vacuum of the precondensation and polycondensation vapor-jet pumps are used, which are operated with TMG vapor, and the vapors sucked off and said TMG vapors are compressed by the vapor jet pumps and condensed by spraying them with a liquid which predominantly consists of TMG, for example the condensate from these spray condensers and optionally fresh make-up TMG.

The feed amount of titanium in the first, initial esterification stage preferably is in the range from 5 to 25 ppm.

As catalytic titanium compound to prepare the catalyst liquid there may preferably be used titanium tetrabutylate or titanium tetraisopropylate. As advantageous catalytic titanium compounds there may for instance also be used any catalytic titanium compound, such as titanium alkylates and their derivatives, like tetra-(2-ethylhexyl)-titanate, tetrastearyl titanate, diisopropoxy-bis-(acetyl-acetonato)-titanium, di-n-butoxy-bis-(triethanolaminato)-titanium,

tributyl monoacetyltitanate, triisopropyl monoacetyltitanate or tetrabenzoic acid titanate, titanium complex salts, like alkali titanium oxalates and malonates, potassium hexafluorotitanate, or titanium complexes with hydroxycarboxylic acids such as tartaric acid, citric acid or lactic acid. Also special catalysts as titanium dioxide - silicon dioxide - co-precipitate or hydrated alkaline containing titanium dioxide can be used.

10 The solvent which is used in the liquid catalyst feed is TMG, in which for stabilization reasons a C_4 to C_{12} dicarboxylic acid is dissolved in quantities below its saturation concentration at ambient temperature. A further embodiment consists in that in TMG C_2 to C_{12} monocarboxylic acid is dissolved below its saturation concentration

20 The organic di-acid which is preferably used for the liquid catalyst feed is selected from terephthalic acid, isophthalic acid or another C_4 - C_{12} aromatic or aliphatic dicarboxylic acid. Preferably the C_4 to C_{12} dicarboxylic acid is incorporated in the PTT and does not act as chain stopper.

25 As further embodiment of the invention the catalyst liquid can be a Ti containing liquid reaction product from TPA and TMG with a degree of esterification of at least 97%. This product is recycled from a later reactor stage and mixed to the first, initial esterification process together with the raw materials. In the continuous process the recycled product amounts to 5 to 40 wt-%, more preferably to 10 to 30 wt-% of the nominal throughput. In the case of the batch process the amount of recycled product lies between 25 and 85 wt-%, preferably between 35 and 70 wt-% of the nominal batch size. This option of the invention is including reaction products which may be withdrawn at any point between the exit from the second stage of esterification and the entry in the polycondensation, and which are used

as liquid catalyst feed for the first initial esterification stage.

5 The second portion of the catalyst may be fed after the esterification step.

10 An important aspect of the invention consists in that in the initial stage of esterification a specific combination of parameters is used. The described special catalyst liquid is well proven at temperatures within the range of 245 to 260°C, an elevated molar feed ratio of TMG to TPA between 1,5 and 2,4 and a pressure of 1 to 3,5 bar. At this conditions only a minor formation of non-filterable particles occurs independently whether delustering agents, 15 like TiO_2 , or other additives are used. This is particularly necessary in the production of fibers.

20 In accordance with a further preferred aspect of the invention, the first initial stage of esterification is conducted to a TPA conversion of 90 to 95%, and the at least second stage of esterification rises the TPA conversion to 97 up to 99%. Latest in the second stage of esterification it has been assured that the last particles of solid TPA from 25 the paste are completely dissolved and the melt is clear and bright.

30 The catalyst liquid introduced into the second or further stages of esterification is preferably a clear solution. These above mentioned conditions enable low filter values of the PTT.

35 The process can be a continuous or a batch process. In the discontinuous process the initial process cycle with a transiently heterogeneous reaction mixture and a limited TPA-conversion of below 95% is considered as the first, initial stage of esterification, while the later reaction

cycle in a homogeneous melt phase at a TPA-conversion of at least 97% represents the at least one subsequent esterification stage. Accordingly the second part of the liquid catalyst feed is added when the TPA has been
5 esterified to at least 95%, preferably to more than 97%.

The precondensation, especially in the continuous process, is favourably split into two pressure sections to provide
10 an optimum condensation progress. The first stage of precondensation is performed between 50 and 150 mbar, the second stage between 2 and 10 mbar.

It is particularly advantageous when the polycondensation
15 of the prepolymer melt is performed at a pressure of 0.3 to 0.8 mbar. Preferably the polycondensation reactor is a disc ring reactor or a cage type reactor, which allows the formation of steadily renewed, large film surfaces of the reaction product and facilitates by this the evaporation of
20 the split products. Under these conditions, increased intrinsic viscosities in the range from 0.75 to 1.15 dl/g are possible.

It was surprisingly found out that in accordance with the inventive process very advantageous filter values of 0 to
25 40 bar·cm²/kg can be realized (determination of filter value see below).

In accordance with a further object of the invention it is provided that the condensates of the spray condensers, optionally after the distillation of low boilers, are
30 recirculated into the first initial and possibly further stages of esterification. In this way, a substantial reduction of the losses in raw materials is achieved.

In accordance with a further preferred embodiment of the
35 invention it is provided that the PTT contains up to 20 wt-% comonomer units derived from other dicarboxylic acids and/or diols. As other dicarboxylic acid there may for

instance be used adipic acid, isophthalic acid or naphthalene dicarboxylic acid. As diols there may for instance be used ethylene glycol, diethylene glycol, triethylene glycol, butylene glycol, polyglycols as well as
5 cyclohexane dimethanol. In this way, the end product can be adapted to the respective application relatively easily.

A further embodiment of the invention consists in that at any point before the end of the polycondensation in the
10 melt phase usual additives such as delustering agents and/or color agents and/or branching agents and/or stabilizers can be added. By means of this measure, the number of the applications of the end product will be increased in connection with a particular viscosity
15 adjustment.

In accordance with the invention, a polyester-soluble cobalt compound, for instance cobalt acetate and/ or polyester soluble organic dyes can be used as color agent
20 or blue toner. As stabilizer a phosphorus compound is added with up to 20 ppm phosphorus, based on PTT, in connection with the cobalt compound and up to 10 ppm phosphorus without any addition of cobalt. By this amounts of phosphorus the catalysis of the thermal degradation of the
25 PTT melt by ions of heavy metals including of the cobalt is stopped because of the formation of neutral phosphorus salts. In special cases the addition of phosphorus may be omitted completely; this depends on the quality of the raw materials, the construction materials of the equipment as
30 well as on the final product application.

A further aspect of the invention consists in that optionally carboxylic acids with three or more COOH groups, polyfunctional acid anhydrides, or polyfunctional alcohols
35 with three or more OH groups, or carboxyphosphonic acids or the esters thereof in concentrations below 5000 ppm are used as branching agents. For polycarboxylic acids and

polyalcohols in most cases concentrations below 1000 ppm are sufficient. These compounds can particularly be used for adjusting or raising the intrinsic viscosity simultaneously.

5

The PTT can be directly processed to fibers, films or other molded materials. In accordance with a further embodiment of the invention it is provided that after the polycondensation in the melt phase the PTT is granulated and crystallized.

10

The resulting granulate can also be thermally treated in the solid state for further IV build up or for devolatilizing low molecular organic products such as acrolein, allyl alcohol and water. The PTT granulate can then be processed to fibers, filaments, films or molded articles.

15

The processed products, i.e. fibers, filaments, films, molded articles or chips, are characterized by an IV of 0.8 to 1.1 dl/g, a filterability of $< 40 \text{ bar} \cdot \text{cm}^2/\text{kg}$ and a thermal stability (as defined below) of $> 80\%$.

20

The subject-matter of the invention will be explained in detail with reference to the following examples.

25

In all examples, the intrinsic viscosities (IV) were determined with a solution of 0.5 g polyester in 100 ml of a mixture of phenol and 1,2-dichlorobenzene (3:2 parts by weight) at 25°C.

30

The COOH terminal group concentration was determined by photometric titration with 0.05 n ethanolic potassium hydroxide solution against bromothymol blue of a solution of polyester in a mixture of o-cresol and chloroform (70 : 30 parts by weight).

35

The measurement of the polymer color values was made on crystallized polyester granules (crystallization at $150 \pm 5^\circ\text{C}/1\text{ h}$) in a tristimulus colorimeter containing three photoelectric cells with a red, green or blue filter. The color values were calculated from the parameters X, Y and Z according to CIELAB.

The filtration behavior of the product melts was determined as follows: PTT dried for 13 h at 130°C and a reduced pressure of $< 1\text{ mbar}$ was molten in a laboratory extruder and metered through a disc filter with a mesh size of $15\text{ }\mu\text{m}$ and a filter area of 2.83 cm^2 by means of a gear pump at a temperature of 260°C . The increase in pressure before the filter was recorded in relation to the amount of melt conveyed and the filterability is calculated as filter value (FV):

$$\text{FV} = \text{filter pressure}[\text{bar}] \cdot \text{filter area}[\text{cm}^2] / \text{amount of melt}[\text{kg}]$$

The thermal stability (TS) of the PTT melt was determined by measuring the intrinsic viscosity of the PTT chips dried for 13 h at 130°C and a reduced pressure of $< 1\text{ mbar}$ as IV_0 before and as IV_T after tempering of the dried chips over one hour at a reference temperature of 255°C in a closed tube under nitrogen.

$$\text{TS} [\%] = 100 \cdot IV_T / IV_0$$

The stated concentrations of the catalysts and additives used in the following examples are defined as parts per million (ppm) referring to the TPA feed.

The catalyst solutions used in the examples according to the invention were prepared as follows:

Catalyst preparation A:
(TPA-stabilized TMG solution)

Because of the hygroscopic properties of TMG, the catalyst solutions were preferably prepared and stored under nitrogen atmosphere.

5

TMG was preheated to 80°C. 50 mg TPA per kg TMG were added while stirring, and stirring was continued until a clear solution was obtained after 20 minutes. The TMG/TPA solution was cooled to about 30 °C.

10

The titanium tetrabutylate was metered with a dropping funnel to the cold, clear acidified TMG solution while stirring. There was thus produced a solution of 2% titanium tetrabutylate in acidified TMG, which was used in this form. When the first drops of titanium tetrabutylate were added, the TMG solution turned light yellow. Remarkably, this color did not change anymore during the further addition of titanium tetrabutylate.

15

20

Catalyst preparation B:
(IPA-stabilized TMG solution)

25

The TMG was preheated to about 60°C. Then a clear solution of 500 mg IPA per kg TMG was produced by stirring. This concentrated solution was cooled to about 30°C. Before adding the titanium tetrabutylate the cooled solution was diluted with fresh TMG in a ratio of 1:4. Thus, the concentration of IPA in the finished solution was 100 mg IPA per kg TMG.

30

The addition of the titanium tetrabutylate to the TMG/ IPA solution was performed in the same way as for preparation A.

35

The invention is illustrated in the following examples.

The results of the examples are summarized together with the fed concentrations of catalyst and additives in the table. examples 1, 2 and 4 are comparative examples.

5 Example 1-3 (Batch process)

10 In this batchwise production of PTT a part of prepolymer from a preceding, prepolymer batch in a quantity of about 42 wt-% of the nominal batch size was kept back in the esterification reactor for the next reaction cycle for stirring the esterification product and for feeding and heating the raw materials TMG and TPA as a paste including the esterification catalyst and optionally cobalt acetate as color agent. The molar TMG to TPA feed ratio of the
15 paste is listed in the table.

20 The quantity of TPA fed into the esterification reactor was 180 kg. The feeding time was 130 minutes. The total cycle time of esterification in example 1-2 was 160 minutes at a temperature of 265°C and a pressure of 1000 mbar (abs.). A column disposed subsequent to the esterification reactor was used for separating the low-boiling compounds, mainly process water, from the trimethylene glycol in the vapors from the esterification, and for the recirculation of the
25 distilled TMG to the process all the time of esterification. The precondensation was carried out in 30 minutes at a simultaneous pressure reduction to 50 mbar (abs.). Thereafter, the prepolymer melt was transferred to a disc ring reactor, and the polycondensation was started
30 by agitating defined by a standard program of speed control and further reducing the pressure within 45 minutes to 0.5 mbar as final pressure. The polycondensation temperature in example 1-2 increased from 260 to 268°C. The total duration of polycondensation indicated in the table
35 corresponded to the maximum viscosity of the polymer possible under the selected conditions, i.e. if the polycondensation was further continued, the intrinsic

viscosity of the polymer decreased again due to the predominance of the thermal degradation reactions. Upon reaching the viscosity maximum, the polycondensation was stopped. At an applied pressure of 55 to 60 bar the polymer melt was discharged from the reactor and granulated.

Special feed conditions within example 1 (comparative)

In example 1, titanium dioxide/silicon dioxide co-precipitate containing 80 mole-% TiO_2 with 50 ppm Ti was fed to the paste as esterification catalyst. In addition, cobalt acetate with 40 ppm Co was added to the paste. Before starting of the precondensation, phosphoric acid with 40 ppm P was added to the melt and after further 2 minutes antimony triacetate with 250 ppm Sb was added as polycondensation catalyst.

Special feed conditions within example 2 (comparative)

In example 2, titanium tetrabutylate with 75 ppm Ti was fed to the paste as esterification catalyst. Before start of the precondensation reaction in the esterification reactor, antimony triacetate with 200 ppm Sb was added as polycondensation catalyst.

Selected process conditions and quality values of the polytrimethylene terephthalate obtained are listed in the following table. In the comparative process very high amounts of catalyst up to 300 ppm were required. In the following inventive examples 80 ppm Ti were sufficient at comparable process times. The process results of the Comparative examples show a deficit with regard to the possible IV- build-up, the thermostability and the filterability.

Special conditions within example 3 (inventive)

According to example 3, TMG and commercially available TPA in a molar ratio of 1.3 were continuously fed into a paste mixer; additionally 15 ppm titanium were added via a catalyst liquid of titanium tetrabutylate in TMG containing TPA according to catalyst preparation A. The resulting paste was fed into the esterification reactor over 130 minutes and reacted batchwise (similar to example 1 and 2). The reaction was performed at an increased pressure of 2000 mbar and at a temperature of 255°C during a cycle time of 160 minutes. The column of the esterification was operated at a molar recycling ratio of TMG to TPA of 0.1 to 0.9, which ratio passed through a maximum during the esterification time. The average total molar feed ratio of TMG to TPA in the esterification reactor was about 1.8.

For completion of the esterification, the reactor pressure was reduced to 1000 mbar within 15 minutes and the esterification was continued in the later stage while stirring at 1000 mbar for 30 minutes. At 5 minutes before starting the vacuum program 65 ppm titanium were added to the esterification product as polycondensation catalyst via the catalyst liquid of preparation A at steady stirring of the product mixture. The subsequent precondensation was carried out during 30 minutes at a temperature of 255 °C and a simultaneous reduction of the pressure to 100 mbar. Subsequently, the melt was transferred to a disc ring reactor, where it was polycondensated at an increasing temperature of 251 - 262°C at a dwell time of 165 minutes and a final pressure of 0.5 mbar. Thereafter the melt was discharged and granulated to PTT chips.

This example clearly illustrates according to the table that under batch conditions, when using the conditions described in the present invention, a stable PTT with an IV of 1.1 dl/g and a filter value of 27 bar·cm²/kg can be produced. The relatively low concentration of carboxyl endgroups in the PTT indicated that no remarkable polymer

degradation during discharge of the PTT occurred. The thermal stability of the PTT enabled a problem-free extrusion and spinning or molding to obtain high quality PTT products.

5

Example 4 to 8(continuous process)

Example 4 (comparative)

- 10 TMG and commercially available TPA in a molar ratio of 1.16 were continuously fed to a paste mixer, and a paste was produced. The catalyst concentration in the paste was 15 ppm titanium. As catalyst titanium tetrabutylate was used as a
- 15 10% mixture with TMG. The paste was continuously fed into the initial esterification reactor and reacted at a pressure of 1000 mbar and a temperature of 255°C for a mean dwell time of 172 minutes under stirring and steady TMG reflux from the esterification column. Into the transfer
- 20 line to a subsequent stirred esterification stage, a second portion of the catalyst (10% titanium tetrabutylate in TMG) with 65 ppm Ti was added, and the product was further esterified in the subsequent esterification stage at a pressure of 1000 mbar, a temperature of 255°C with a mean
- 25 dwell time of 60 minutes. The esterification product was transferred into a third reaction stage also equipped with a stirrer for precondensation at 100 mbar and 255 °C within 30 minutes.
- 30 Likewise the precondensation was completed in a further stage at 7 mbar, 257°C within 35 minutes. The precondensate, showing an IV of 0.26 dl/g was transferred to a disc ring reactor by means of a gear-type metering pump for the final polycondensation at a vacuum of 0.5
- 35 mbar, a mean dwell time of 150 minutes, an increasing temperature profile of

258-264°C and an agitator speed of 5.5 rpm. From the disc ring reactor, the melt was discharged and granulated.

The PTT thus produced had an intrinsic viscosity of 0.92 dl/g and a filter value of 143 bar·cm²/kg. The higher concentration of carboxyl endgroups in the PTT indicated another, from the invention different polymer formation, whereas the thermal properties of the products were similar. Polymers with such high filter values entail to a short service life of the filter in the spinning process, and are not suitable for the production of fibers and filaments.

Example 5

In example 5, the conditions for the production of PTT corresponded to example 4 with following exceptions. The molar ratio TMG:TPA in the paste was risen to 1.3; the catalyst concentration in the paste was 15 ppm titanium. As catalyst liquid the catalyst preparation B was used. The paste was continuously fed into the first initial esterification reactor and reacted while stirring at a pressure of 2000 mbar and a temperature of 255°C for a mean dwell time of 172 minutes. The molar reflux from the column of the esterification amounted to 0.8 moles TMG per TPA; by this a total molar ratio of TMG to TPA of 2.1 was present. After the continuous transfer to a second subsequent esterification stage, a further amount of catalyst of 65 ppm Ti was added into the mixed esterification product in form of the catalyst preparation B. The esterification in the second stage, the precondensation and the polycondensation were performed at conditions identical to those in example 4.

The PTT thus produced had an intrinsic viscosity of 0.93 dl/g and a filter value of 5 bar·cm²/kg. The good filter value of the intermediate prepolymer sample of 8

bar•cm²/kg, already indicated a good filterability of the melt. In the PTT production process and in the production of fibers and filaments this offers great economic advantages due to a long service life of the filter.

5

Example 6

Similar to example 5, TMG and TPA were continuously fed into the paste mixer in a molar ratio of 1.25. Thereby 70 wt-% of the TMG used consisted of recycled TMG collected from the vapor condensers of different stages. The concentration of solids (a mixture of PTT oligomers) in the recycled TMG was 2.5 wt-%. In addition, 15 ppm titanium as catalyst solution, preparation B, and 20 ppm Co as cobalt acetate were added to the raw material paste, and the paste was pumped to the initial esterification stage. The total molar TMG to TPA feed ratio including the TMG- reflux from the column was 1.9. All other process conditions in esterification, precondensation and polycondensation were selected in accordance with example 4. According to example 5, additional 65 ppm Ti were added into the mixed esterification product of the subsequent second esterification stage. As catalyst liquid feed was used preparation B. Additionally 20 ppm P (as solution of phosphoric acid in TMG) were dosed into the transfer line of the esterification product to the first precondensation stage.

The granulated PTT had a viscosity of 0.918 dl/g and a filter value of 7 bar•cm²/kg.

Example 7:

Example 7 was performed in a similar way as example 6, and for the production of paste there was likewise used recycled TMG. The molar ratio TMG to TPA was 1.25. 46 wt-%

of the TMG present in the feed paste were recycled TMG with a content of oligomeric solids of 2.2 wt-%. Different to example 6, 10 ppm Co as cobalt acetate and 5 ppm P as phosphoric acid were added to the paste. The catalyst feed into the paste was 15 ppm Ti as catalyst liquid preparation A. The polycondensation catalyst was added in an amount of 65 ppm Ti, as catalyst liquid preparation A to the melt of the subsequent second esterification stage. The other process conditions were as following:

Total TMG/TPA - mol ratio= 1.9

1 st	Esterification stage:	249°C	2000 mbar	230 min
2 nd	Esterification stage:	248°C	1000 mbar	30 min
1 st	Prepolycond. stage:	247°C	80 mbar	37 min
2 nd	Prepolycond. stage:	247°C	8 mbar	41 min
	Polycondensation stage:	247-260°C	0.3 mbar	220 min

Under these process conditions a PTT was obtained with an IV of 0.93 dl/g, a high thermal stability and a good filterability.

Example 8

(Continuous process with recirculation of the melt from esterification 2 to esterification 1)

TMG and TPA were continuously fed into the paste mixer in a molar ratio of 1.25. Thereby, 58 wt-% of the TMG used consisted of recycled TMG with 2 wt-% of oligomeric solids. After achieving stationary flow conditions the TMG/TPA feed paste without any catalyst was transferred to the first, initial stirred esterification stage. At the same time a separate partial recycling stream of 19 wt-% of the product from the subsequent second esterification stage to the first initial stage containing the catalyst as a diluted

solution in a prereacted homogenous product mixture with an increased degree of esterification of about 97,5%.

5 The actual catalyst addition to the second esterification stage was carried out with 80 ppm Ti (based on PTT) as liquid catalyst preparation B. As a consequence of the partial product recycling from the second subsequent esterification stage into the initial esterification stage the relative throughput per 100 wt-% product was in both
10 esterification stages increased to 119 wt-% and the average residence times were decreased to 135 and 48 minutes. The total molar TMG to TPA feed ratio to the esterification was 2.0. Further conditions were:

15 1st esterification stage: 255°C 1800 mbar
2nd esterification stage: 255°C 1000 mbar.

The process conditions in the precondensation and polycondensation were the same as in example 4. The final
20 PTT product showed an IV of 0.913 dl/g, a good thermal stability, and a good filterability, in accordance with the invention.

Claims:

1. A process of producing polytrimethylene terephthalate (PTT) with an intrinsic viscosity of at least 0.75 dl/g by esterification of terephthalic acid (TPA) with tri-
5 methylene glycol (TMG) in the presence of a catalytic titanium compound to obtain an esterification product, precondensation of the esterification product to obtain a precondensation product and polycondensation of the
10 precondensation product to obtain PTT, characterized in that

a) the esterification is performed in at least two stages, a first, initial stage and at least one second, subsequent
15 stage connected to a process column,

b) a liquid catalyst feed is prepared on base of TMG having a concentration of less than 5 wt-% titanium in the form of a titanium compound stabilized by a bifunctional
20 organic acid,

c) a major quantity between 65 and 100% of said liquid catalyst feed containing 35 to 110 ppm titanium, is introduced into the at least one subsequent esterifi-
25 cation stage, operated at a temperature of 245 to 260°C, and a pressure of 0.7 to 1.2 bar,

d) a minor quantity of said liquid catalyst feed containing 0 to 40 ppm titanium and equal in maximum to 35%
30 of the total catalyst is directly fed to the initial esterification stage usually together with the raw materials, which direct catalyst feed can be partially or completely sub stituted by the same quantity of catalyst in a reaction product, which may be recycled from any further
35 reaction stages and which is mixed to the raw materials for further reaction in said initial esterification stage in connection with a total molar TMG to TPA feed ratio of 1.15

to 2.5, a temperature of 240 to 270 °C and a pressure of 1 - 3.5 bar,

5 e) the precondensation is performed at a temperature of 245 to 260°C under a reduced pressure between 2 and 200 mbar,

10 f) the polycondensation is carried out in the melt phase at a pressure of 0.2 to 2.5 mbar, a temperature of 252 to 267°C, basically increasing from the entry to the exit of the polycondensation reactor during agitation and formation of steadily renewed, large film surfaces of the reaction product for evaporation of the split products, and

15 g) for generating the vacuum to perform the precondensation and polycondensation vapor-jet pumps are used to remove the released TMG and PTT oligomers and low boilers from the gas phase of the reactors, and the vapor-jet pumps are operated with TMG vapor, and the vapors
20 sucked off and compressed by the vapor-jet pumps and said TMG vapors are condensed by spraying them with a liquid which predominantly consists of TMG.

25 2. A process as claimed in claim 1, characterized in that said titanium compound is a titanium alkylate, like titanium tetrabutylate, titanium tetraisopropylate or tetra-(2-ethylhexyl)-titanate, or a titanium dioxide - silicon dioxide - co-precipitate or a hydrated sodium containing titanium dioxide or a titanium salt of organic
30 acids or a titanium complex with hydroxycarboxylic acids.

35 3. A process as claimed in any of claims 1 to 2, characterized in that said liquid catalyst feed contains trimethylene glycol, in which a C₄ to C₁₂ dicarboxylic acid is dissolved below its saturation concentration.

4. The process as claimed in claim 3, characterized in that terephthalic acid or isophthalic acid is used as C_4 to C_{12} dicarboxylic acid.

5 5. The process as claimed in any of claims 1 to 2 characterized in that said liquid catalyst feed contains tri-methyleneglycol, in which a C_2 to C_{12} monocarboxylic acid is dissolved below its saturation concentration.

10 6. A process as claimed in any of claims 1 to 5, characterized in that the process is a continuous process.

15 7. A process as claimed in claim 6, characterized in that a part of the reaction product is withdrawn at any point between the exit of the subsequent stage of esterification and the entry to the polycondensation and mixed to the raw materials by recycling said reaction product to the first, initial esterification stage.

20 8. A process as claimed in claim 7, characterized in that said reaction product recycled to the initial esterification stage lies in the range of 5 to 40 wt-% of the nominal throughput.

25 9. A process as claimed in any of claims 1 to 5, characterized in that the process is a discontinuous process, and the initial process cycle with a transiently heterogeneous reaction mixture and a limited TPA-conversion of below 95% represents said 'initial stage' and the later
30 reaction cycle in a homogeneous melt phase with a TPA conversion of at least 97% represents said 'subsequent stage' of the esterification process, to which the major part of the catalyst is fed, and a portion of the reaction product kept back at the end of the precondensation is used
35 for the next discontinuous process in step d as catalyst containing reaction product.

10. A process as claimed in any of claims 1 to 9 characterized in that the second portion of the catalyst is fed after the esterification step.

5 11. A Process as claimed in claim 9, characterized in that said catalyst containing reaction product recycled to the initial esterification stage lies in a range of 25 to 85 wt-% of the nominal batch size.

10 12. A process as claimed in any of claims 1 to 11, characterized in that the first, initial stage of esterification is conducted to a degree of esterification of 90 to 95%, and the subsequent stage of esterification is conducted to a degree of esterification of 97 to 99%.

15 13. A process as claimed in any of claims 1 to 12, characterized in that the condensed vapors from step g are recirculated to the initial and possibly further subsequent stages of the esterification, optionally after removing of
20 the low boilers from TMG by distillation.

14. A process as claimed in any of claims 1 to 13, characterized in that the PTT contains up to 20 wt-% comonomer units derived from other dicarboxylic acids
25 and/or diols.

15. A process as claimed in any of claims 1 to 14, characterized in that at any point before the end of the polycondensation in the melt phase usual additives such as
30 delustering agents and/or color agents and/or branching agents and/or stabilizers are added.

16. A Process as claimed in any of claims 1 to 15, characterized in that said polycondensation reactor is a
35 discring reactor or a cage type reactor.

17. A process as claimed in any of claims 1 to 16,
characterized in that the PTT is after the polycondensation
in the melt phase granulated to chips, and the chips are
5 dried, crystallized and treated thermally in the solid
phase.

18. A process as claimed in any of claims 1 to 17,
characterized in that the PTT is processed to products,
10 like fibers or filaments or films or molded articles or
chips.

19. A process as claimed in claims 18, characterized in
that the processed products have an IV of 0.8 to 1.1 dl/g,
15 a filterability of $< 40 \text{ bar} \cdot \text{cm}^2/\text{kg}$ and a thermal stability
(as defined before) of $> 80\%$.

INTERNATIONAL SEARCH REPORT

Int. Application No.

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A. CLASSIFICATION OF SUBJECT MATTER

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B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C08G

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ, CHEM ABS Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	CHEMICAL ABSTRACTS, vol. 81, no. 24, 16 December 1974 (1974-12-16) Columbus, Ohio, US; abstract no. 153134, IKEUCHI, HIROYIKI ET AL.: "Catalysts for manufacture of poly(tetramethyleneterephthalate)" XP002115471 abstract & JP 49 057092 A (TORAY INDUSTRIES) 3 June 1974 (1974-06-03)	1
A	US 5 656 716 A (SCHMIDT WOLFGANG ET AL) 12 August 1997 (1997-08-12) claims 1-11; example 16 -/-	1-5, 18, 19

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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INTERNATIONAL SEARCH REPORT

International Application No

PGT/EP 00/03474

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 466 776 A (KRAUTSTRUNK JUERGEN ET AL) 14 November 1995 (1995-11-14) claims 1-13	1-19
A	US 5 872 204 A (KUO TUNG-YING ET AL) 16 February 1999 (1999-02-16) abstract; claims 1-27	1-5, 18, 19
A	EP 0 431 977 A (DU PONT) 12 June 1991 (1991-06-12) claims 1-17	1

INTERNATIONAL SEARCH REPORT

Information on patent family members

Inventor's Application No

PCT/EP 00/03474

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
JP 49057092 A	03-06-1974	NONE	
US 5656716 A	12-08-1997	DE 19513056 A EP 0736560 A	10-10-1996 09-10-1996
US 5466776 A	14-11-1995	DE 4419397 A DE 59505625 D EP 0685502 A ES 2129701 T	14-12-1995 20-05-1999 06-12-1995 16-06-1999
US 5872204 A	16-02-1999	NONE	
EP 0431977 A	12-06-1991	US 5015759 A CA 2031611 A JP 2894543 B JP 7053464 A JP 2031681 C JP 4108760 A JP 7039372 B KR 178061 B SG 54304 A	14-05-1991 09-06-1991 24-05-1999 28-02-1995 19-03-1996 09-04-1992 01-05-1995 15-05-1999 16-11-1998



Am 17. 04. 2000

per Fax
vorab an

das EPA, München

PCT zur Kasse

ANTRAG

393745

21986

Der Unterzeichnete beantragt, daß die vorliegende internationale Anmeldung nach dem Vertrag über die internationale Zusammenarbeit auf dem Gebiet des Patentwesens behandelt wird.

Von	Ideamt auszufüllen
PCT/EP	0 0 / 0 3 4 7 4
Internationales Aktenzeichen	
17 APR 2000	(17. 04. 2000)
Internationales Anmeldedatum	
EPA/EP - PATENT OFFICE PCT INTERNATIONAL APPLICATION Name des Anmeldeamts und "PCT International Application"	
Aktenzeichen des Anmelders oder Anwalts (falls gewünscht) (max. 12 Zeichen) 990070PCT	

Feld Nr. I BEZEICHNUNG DER ERFINDUNG

Process of producing polytrimethylene terephthalate (PTT)

Feld Nr. II ANMELDER

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

LURGI ZIMMER AG
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Deutschland

☐ Diese Person ist gleichzeitig Erfinder

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Telefaxnr.:
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Fernschreiber
-

Staatsangehörigkeit (Staat):

DE

Sitz oder Wohnsitz (Staat):

DE

Diese Person ist Anmelder für folgende Staaten:

☐

alle Bestimmungsstaaten

☒

alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☐

nur die Vereinigten Staaten von Amerika

☐

die im Zusatzfeld angegebenen Staaten

Feld Nr. III WEITERE ANMELDER UND/ODER (WEITERE) ERFINDER

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Shell Internationale Research Maatschappij B.V.
Carel van Bylandt Laan 30,
NL-2596 HR The Hague
Netherlands

Diese Person ist:

☐ nur Anmelder

☒ Anmelder und Erfinder

☐ nur Erfinder. Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.

Staatsangehörigkeit (Staat):

NL

Sitz oder Wohnsitz (Staat):

NL

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☐

alle Bestimmungsstaaten

☒

alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☐

nur die Vereinigten Staaten von Amerika

☐

die im Zusatzfeld angegebenen Staaten

☒ Weitere Anmelder und/oder (weitere) Erfinder sind auf einem Fortsetzungsblatt angegeben

Feld Nr. IV ANWALT ODER GEMEINSAMER VERTRETER; ODER ZUSTELLANSCHRIFT

Die folgende Person wird hiermit bestellt, um für den (die) Anmelder vor den zuständigen internationalen Behörden in folgender Eigenschaft zu handeln als

☐

Anwalt

☒

gemeinsamer Vertreter

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben.)

Veronika R e v e s z (RA)
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Fernschreiber

-

☐ Zustellanschrift: Dieses Kästchen ist anzukreuzen, wenn kein Anwalt oder gemeinsamer Vertreter bestellt ist und statt dessen im obigen Feld eine spezielle Zustellanschrift angegeben ist.

Fortsetzung von Feld Nr. III WEITERE ANMELDER UND/ODER (WEITERE) ERFINDER

Wird keines der folgenden Felder benutzt, so sollte dieses Blatt dem Antrag nicht beigelegt werden.

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

WILHELM, Fritz
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Deutschland

Diese Person ist:

☐ nur Anmelder

☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

Staatsangehörigkeit (Staat):

DE

Sitz oder Wohnsitz (Staat):

DE

Diese Person ist Anmelder für folgende Staaten:

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☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

SEIDEL, Eckhard
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Diese Person ist:

☐ nur Anmelder

☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

Staatsangehörigkeit (Staat):

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Sitz oder Wohnsitz (Staat):

DE

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☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

REITZ, Hans
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Diese Person ist:

☐ nur Anmelder

☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

Staatsangehörigkeit (Staat):

DE

Sitz oder Wohnsitz (Staat):

DE

Diese Person ist Anmelder für folgende Staaten:

☐ alle Bestimmungsstaaten

☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

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☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

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DE

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☐ die im Zusatzfeld angegebenen Staaten

☒ Weitere Anmelder und/oder (weitere) Erfinder sind auf einem zusätzlichen Fortsetzungsblatt angegeben.

Fortsetzung von Feld Nr. III WEITERE ANMELDER UND/ODER (WEITERE) ERFINDER

Wird keines der folgenden Felder benutzt, so sollte dieses Blatt dem Antrag nicht beigelegt werden.

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

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☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

Staatsangehörigkeit (Staat):

DE

Sitz oder Wohnsitz (Staat):

DE

Diese Person ist Anmelder für folgende Staaten:

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☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

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U S A

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☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

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BLACKBOURN, Robert Lawrence
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U S A

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☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

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☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

Name und Anschrift: (Familienname, Vorname; bei juristischen Personen vollständige amtliche Bezeichnung. Bei der Anschrift sind die Postleitzahl und der Name des Staats anzugeben. Der in diesem Feld in der Anschrift angegebene Staat ist der Staat des Sitzes oder Wohnsitzes des Anmelders, sofern nachstehend kein Staat des Sitzes oder Wohnsitzes angegeben ist.)

TOMASKOVIC, Robert Stephan
7615 Foster Creek Drive
Richmond, Tx. 77469
U S A

Diese Person ist:

☐ nur Anmelder

☒ Anmelder und Erfinder

☐ nur Erfinder (Wird dieses Kästchen angekreuzt, so sind die nachstehenden Angaben nicht nötig.)

Staatsangehörigkeit (Staat):

US

Sitz oder Wohnsitz (Staat):

US

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☐ alle Bestimmungsstaaten

☐ alle Bestimmungsstaaten mit Ausnahme der Vereinigten Staaten von Amerika

☒ nur die Vereinigten Staaten von Amerika

☐ die im Zusatzfeld angegebenen Staaten

☐ Weitere Anmelder und oder weitere Erfinder sind auf einem zusätzlichen Fortsetzungsblatt anzugeben



Feld Nr. V BESTIMMUNG VON STAATEN

Die folgenden Bestimmungen nach Regel 4.9 Absatz a werden hiermit vorgenommen (bitte die entsprechenden Kästchen ankreuzen; wenigstens ein Kästchen muß angekreuzt werden):

Regionales Patent

- ☐ AP ARIPO-Patent: GH Ghana, GM Gambia, KE Kenia, LS Lesotho, MW Malawi, SD Sudan, SZ Swasiland, UG Uganda, ZW Simbabwe und jeder weitere Staat, der Vertragsstaat des Harare-Protokolls und des PCT ist
- ☐ EA Eurasisches Patent: AM Armenien, AZ Aserbaidshan, BY Belarus, KG Kirgisistan, KZ Kasachstan, MD Republik Moldau, RU Russische Föderation, TJ Tadschikistan, TM Turkmenistan und jeder weitere Staat, der Vertragsstaat des Eurasischen Patentübereinkommens und des PCT ist
- ☐ EP Europäisches Patent: AT Österreich, BE Belgien, CH und LI Schweiz und Liechtenstein, CY Zypern, DE Deutschland, DK Dänemark, ES Spanien, FI Finnland, FR Frankreich, GB Vereinigtes Königreich, GR Griechenland, IE Irland, IT Italien, LU Luxemburg, MC Monaco, NL Niederlande, PT Portugal, SE Schweden und jeder weitere Staat, der Vertragsstaat des Europäischen Patentübereinkommens und des PCT ist
- ☐ OA OAPI-Patent: BF Burkina Faso, BJ Benin, CF Zentralafrikanische Republik, CG Kongo, CI Côte d'Ivoire, CM Kamerun, GA Gabun, GN Guinea, GW Guinea-Bissau, ML Mali, MR Mauretanien, NE Niger, SN Senegal, TD Tschad, TG Togo und jeder weitere Staat, der Vertragsstaat der OAPI und des PCT ist (falls eine andere Schutzrechtsart oder ein sonstiges Verfahren gewünscht wird, bitte auf der gepunkteten Linie angeben):

Nationales Patent (falls eine andere Schutzrechtsart oder ein sonstiges Verfahren gewünscht wird, bitte auf der gepunkteten Linie angeben):

- | | |
|---|---|
| <input type="checkbox"/> AL Albanien | <input type="checkbox"/> LS Lesotho |
| <input type="checkbox"/> AM Armenien | <input type="checkbox"/> LT Litauen |
| <input type="checkbox"/> AT Österreich | <input type="checkbox"/> LU Luxemburg |
| <input type="checkbox"/> AU Australien | <input type="checkbox"/> LV Lettland |
| <input type="checkbox"/> AZ Aserbaidshan | <input type="checkbox"/> MD Republik Moldau |
| <input type="checkbox"/> BA Bosnien-Herzegowina | <input type="checkbox"/> MG Madagaskar |
| <input type="checkbox"/> BB Barbados | <input type="checkbox"/> MK Die ehemalige jugoslawische Republik Mazedonien |
| <input checked="" type="checkbox"/> BR Brasilien | <input type="checkbox"/> MN Mongolei |
| <input type="checkbox"/> BY Belarus | <input type="checkbox"/> MW Malawi |
| <input type="checkbox"/> CA Kanada | <input checked="" type="checkbox"/> MX Mexiko |
| <input type="checkbox"/> CH und LI Schweiz und Liechtenstein | <input type="checkbox"/> NO Norwegen |
| <input checked="" type="checkbox"/> CN China | <input type="checkbox"/> NZ Neuseeland |
| <input type="checkbox"/> CU Kuba | <input type="checkbox"/> PL Polen |
| <input type="checkbox"/> CZ Tschechische Republik | <input type="checkbox"/> PT Portugal |
| <input type="checkbox"/> DE Deutschland | <input type="checkbox"/> RO Rumänien |
| <input type="checkbox"/> DK Dänemark | <input type="checkbox"/> RU Russische Föderation |
| <input type="checkbox"/> EE Estland | <input type="checkbox"/> SD Sudan |
| <input type="checkbox"/> ES Spanien | <input type="checkbox"/> SE Schweden |
| <input type="checkbox"/> FI Finnland | <input type="checkbox"/> SG Singapur |
| <input type="checkbox"/> GB Vereinigtes Königreich | <input type="checkbox"/> SI Slowenien |
| <input type="checkbox"/> GD Grenada | <input type="checkbox"/> SK Slowakei |
| <input type="checkbox"/> GE Georgien | <input type="checkbox"/> SL Sierra Leone |
| <input type="checkbox"/> GH Ghana | <input type="checkbox"/> TJ Tadschikistan |
| <input type="checkbox"/> GM Gambia | <input type="checkbox"/> TM Turkmenistan |
| <input type="checkbox"/> HR Kroatien | <input type="checkbox"/> TR Türkei |
| <input type="checkbox"/> HU Ungarn | <input type="checkbox"/> TT Trinidad und Tobago |
| <input type="checkbox"/> ID Indonesien | <input type="checkbox"/> UA Ukraine |
| <input type="checkbox"/> IL Israel | <input type="checkbox"/> UG Uganda |
| <input type="checkbox"/> IN Indien | <input checked="" type="checkbox"/> US Vereinigte Staaten von Amerika |
| <input type="checkbox"/> IS Island | <input type="checkbox"/> UZ Usbekistan |
| <input checked="" type="checkbox"/> JP Japan | <input type="checkbox"/> VN Vietnam |
| <input type="checkbox"/> KE Kenia | <input type="checkbox"/> YU Jugoslawien |
| <input type="checkbox"/> KG Kirgisistan | <input type="checkbox"/> ZW Simbabwe |
| <input type="checkbox"/> KP Demokratische Volksrepublik Korea | |
| <input checked="" type="checkbox"/> KR Republik Korea | |
| <input type="checkbox"/> KZ Kasachstan | |
| <input type="checkbox"/> LC Saint Lucia | |
| <input type="checkbox"/> LK Sri Lanka | |
| <input type="checkbox"/> LR Liberia | |

Kästchen für die Bestimmung von Staaten (nur die Zwecke eines nationalen Patents), die dem PCT nach der Veröffentlichung dieses Formblatts beigetreten sind:

Erklärung bzgl. vorsorglicher Bestimmungen: Zusätzlich zu den oben genannten Bestimmungen nimmt der Anmelder nach Regel 4.9 Absatz b auch alle anderen nach dem PCT zulässigen Bestimmungen vor mit Ausnahme der im Zusatzfeld genannten Bestimmungen, die von dieser Erklärung ausgenommen sind. Der Anmelder erklärt, daß diese zusätzlichen Bestimmungen unter dem Vorbehalt einer Bestätigung stehen und jede zusätzliche Bestimmung, die vor Ablauf von 15 Monaten ab dem Prioritätsdatum nicht bestätigt wurde, nach Ablauf dieser Frist als vom Anmelder zurückgenommen gilt. (Die Bestätigung einer Bestimmung erfolgt durch die Einreichung einer Mitteilung, in der diese Bestimmung angegeben wird, und die Zahlung des Bezugsbetrags, und der Bestätigung gegenüber. Die Mitteilung muß bevor der Frist von 15 Monaten abgelaufen ist.)

Blatt Nr. ... 5 ...

PCT/EP 00 / 03474

Feld Nr. VI PRIORITÄTSANSPRUCH

☐ Weitere Prioritätsansprüche sind im Zusatzfeld angegeben.

Anmeldedatum der früheren Anmeldung (Tag/Monat/Jahr)	Aktenzeichen der früheren Anmeldung	Ist die frühere Anmeldung eine		
		ationale Anmeldung Staat	regionale Anmeldung regionales Amt	internationale Anmeldung Anmeldeamt
Zeile (1) 22. April 1999 (22. 04. 1999)	EP 99 107 370.1	EP		
Zeile (2)				
Zeile (3)				

- ☒ Das Anmeldeamt wird ersucht, eine beglaubigte Abschrift der oben in der (den) Zeile(n) (1) bezeichneten früheren Anmeldung(en) zu erstellen und dem internationalen Büro zu übermitteln (nur falls die frühere Anmeldung(en) bei dem Amt eingereicht worden ist(sind), das für die Zwecke dieser internationalen Anmeldung Anmeldeamt ist)
- * Falls es sich bei der früheren Anmeldung um eine ARIPO-Anmeldung handelt, so muß in dem Zusatzfeld mindestens ein Staat angegeben werden, der Mitgliedsstaat der Pariser Verbandsübereinkunft zum Schutz des gewerblichen Eigentums ist und für den die frühere Anmeldung eingereicht wurde.

Feld Nr. VII INTERNATIONALE RECHERCHENBEHÖRDE

Wahl der internationalen Recherchenbehörde (ISA)
(falls zwei oder mehr als zwei internationale Recherchenbehörden für die Ausführung der internationalen Recherche zuständig sind, geben Sie die von ihnen gewählte Behörde an; der Zweibuchstaben-Code kann benutzt werden):

Antrag auf Nutzung der Ergebnisse einer früheren Recherche; Bezugnahme auf diese frühere Recherche (falls eine frühere Recherche bei der internationalen Recherchenbehörde beantragt oder von ihr durchgeführt worden ist):

Datum (Tag/Monat/Jahr) Aktenzeichen Staat (oder regionales Amt)

ISA /

Feld Nr. VIII KONTROLLISTE; EINREICHUNGSSPRACHE

Diese internationale Anmeldung enthält die folgende Anzahl von Blättern:

Antrag : 5
Beschreibung (ohne Sequenzprotokollteil) : 20
Ansprüche : 5
Zusammenfassung : 1
Zeichnungen : -
Sequenzprotokollteil der Beschreibung : -
Blattzahl insgesamt : 31

Dieser internationalen Anmeldung liegen die nachstehend angekreuzten Unterlagen bei:

- ☒ Blatt für die Gebührenberechnung
- ☐ Gesonderte unterzeichnete Vollmachten folgen
- ☐ Kopie der allgemeinen Vollmacht; Aktenzeichen (falls vorhanden):
- ☐ Begründung für das Fehlen einer Unterschrift
- ☐ Prioritätsbeleg(e) in Feld Nr. VI durch folgende Zeilennummer gekennzeichnet:
- ☐ Übersetzung der internationalen Anmeldung in die folgende Sprache:
- ☐ Gesonderte Angaben zu hinterlegten Mikroorganismen oder anderem biologischen Material
- ☐ Protokoll der Nucleotid- und/oder Aminosäuresequenzen in computerlesbarer Form
- ☐ Sonstige (einzeln auführen):

Abbildung der Zeichnungen, die mit der Zusammenfassung veröffentlicht werden soll (Nr.): -

Sprache, in der die internationale Anmeldung eingereicht wird:

Feld Nr. IX UNTERSCHRIFT DES ANMELDERS ODER DES ANWALTS

Der Name jeder unterzeichnenden Person ist neben der Unterschrift zu wiederholen, und es ist anzugeben, sofern sich dies nicht eindeutig aus dem Antrag ergibt, in welcher Eigenschaft die Person unterzeichnet.

V. Revesz
V. Revesz

1. Datum des tatsächlichen Eingangs dieser internationalen Anmeldung: 17 APR 2000 (17. 04. 2000)		2. Zeichnungen <input type="checkbox"/> eingegangen: <input type="checkbox"/> nicht eingegangen:
3. Geändertes Eingangsdatum aufgrund nachträglich, jedoch fristgerecht eingegangener Unterlagen oder Zeichnungen zur Vervollständigung dieser internationalen Anmeldung:		
4. Datum des fristgerechten Eingangs der angeforderten Richtigstellungen nach Artikel 11(2) PCT:		
5. Internationale Recherchenbehörde (falls zwei oder mehr zuständig sind): ISA /	6. <input type="checkbox"/> Übermittlung des Recherchenexemplars bis zur Zahlung der Recherchegebühr aufgeschoben	

Datum des Eingangs des Aktenexemplars beim Internationalen Büro:

Vom Internationalen Büro auszufüllen

Lurgi Zimmer AG,
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Shell Internationale Research Maatschappij B.V.,
Carel van Bylandt Laan 30,
NL-2596 HR The Hague

Process of producing polytrimethylene terephthalate (PTT)

Description:

— 5 This invention relates to a process of producing polytrimethylene terephthalate (PTT) with an intrinsic viscosity of at least 0.75 dl/g by esterification of terephthalic acid (TPA) with trimethylene glycol (TMG) in the presence of a catalytic titanium compound to obtain an esterification product, precondensation of the esterification product to obtain a precondensation product, and polycondensation of the precondensation product to obtain PTT.

10

Processes of producing PTT are known (U.S. Patents Nos. 2,456,319; 4,611,049; 5,340,909; 5,459,229; 5,599,900).

15

For instance, the U.S. Patent No. 4,611,049 describes the use of a protonic acid as co-catalyst for accelerating the polycondensation, where the addition of p-toluene sulfonic acid in a concentration of 50 mmol-% effects an increase of the maximum achievable intrinsic viscosity of 0.75 dl/g in a batch process catalyzed with 50 mmol-% tetrabutyl titanate to 0.90 dl/g.

20

The U.S. Patent No. 5,340,909 proposes to achieve an improvement of the polycondensation capacity and the color of the polytrimethylene terephthalate by using a tin

catalyst, which together with titanium can already be present in the esterification. Statements on the influence of recirculation of the vapor condensates obtained during the polycondensation on the polycondensation capacity of the reaction melt cannot be found in the U.S. Patent No. 5,340,909.

The U.S. Patent No. 5,459,229 proposes to reduce the concentration of acrolein in the vapors by adding alkalines to the condensates produced during the esterification of trimethylene glycol and terephthalic acid. The U.S. Patent No. 5,459,229 does not contain any details concerning the esterification and polycondensation.

The U.S. Patent No. 5,599,900 describes a process of producing polytrimethylene terephthalate, where in the presence of an inert stripping gas either after the transesterification or after the esterification a polytrimethylene terephthalate with a degree of polymerization of 64 is synthesized. Moreover, it is desired to also adjust higher molecular weights but this is not proven by experiment.

WO 97/23543A describes a process of producing polytrimethylene terephthalate, where it is provided to first of all produce a preproduct with an intrinsic viscosity of 0.16 dl/g by means of transesterification. This preproduct is converted to pastilles by means of dripping, which pastilles directly crystallize at crystallization temperatures up to 130°C. The actual polymer is produced subsequently by solid-phase condensation. It is disadvantageous that a high amount of trimethylene glycol and oligomers gets into the process gas and must be recovered or burnt in an expensive way.

The U.S. Patent No. 5,798,433 describes a process of producing PTT by direct esterification of terephthalic acid

with 1,3-propanediol and subsequent precondensation and polycondensation. The PTT produced contains not more than 5 ppm acrolein and 3 ppm allyl alcohol. It is obtained by esterification in the presence of 30 to 200 ppm titanium in the form of an inorganic esterification catalyst containing at least 50 mol-% TiO_2 as a precipitate, blocking the esterification catalyst after the esterification by adding 10 to 100 ppm phosphorus in the form of an oxygen containing phosphorus compound, and subsequent precondensation and polycondensation in the presence of 100 to 300 ppm antimony in the form of a usual antimony polycondensation catalyst as well as optionally adding usual color agents. The quantity of the required catalyst is very high and causes severe disadvantages in the product quality especially with regard to the thermal product stability.

From U.S. Patent No. 4,011,202 the use of glycol jet pumps is known. However, the use of TMG-jets is not yet detailed.

It is the object of the invention to create a melt phase process of producing PTT with an intrinsic viscosity between 0.75 and 1.15 dl/g and a good thermal stability, and to achieve at the same time an efficiently long service life of the filters when the polymer melt is filtered prior to processing the same to form the end products. The process may be a batch or continuous process. Additionally, the PTT process should also allow the recycling of TMG and oligomer by-products.

The foregoing objects are achieved in accordance with the invention by a process as defined in the claims.

The characteristic features of this process, which comprises the catalytic esterification of TPA with TMG, precondensation of the esterification product and

polycondensation of the precondensation product, are as follows:

- 5 - The esterification is performed in at least 2 stages, one initial stage and at least one second, subsequent stage connected to a process column.
- 10 - The catalyst used for esterification and polycondensation is a titanium compound in a stabilized liquid formulation, which is prepared from a catalytic titanium compound, an organic diacid and TMG as solvent, in such way that the liquid catalyst feed contains less than 5 wt-% titanium.
- 15 - The catalyst used for esterification in the first, initial stage can be alternatively a Ti containing liquid reaction product from TPA and TMG with a degree of esterification of at least 97%, which may be recycled from a later reaction stage and fed to the
20 initial esterification stage together with the raw materials.
- 25 - A defined quantity of the described liquid catalyst feed is introduced into the first, initial esterification stage and separately a second defined quantity of the liquid catalyst feed is added to the at least one subsequent stage of esterification.
- 30 - In the first, initial esterification stage a total molar ratio of TMG / TPA of 1.15 to 2.5, an amount of titanium of 0 to 40 ppm, which is in maximum 35% of the total amount of catalyst, a temperature of 240 to 270°C and an absolute pressure of 1 to 3,5 bar are adjusted, whereby the reaction is continued until 90 to 95% of
35 the TPA are esterified.

- In the at least one subsequent esterification stage an additional amount of titanium of 35 to 110 ppm, which is 65 to 100% of the total amount of catalyst, a temperature of 245 to 260°C and an absolute pressure of 0.7 to 1.2 bar are adjusted, whereby the reaction is continued until 97 to 99% of the TPA are esterified.
- The precondensation is performed at a temperature of 245 to 260°C under a reduced pressure in the range from 2 to 200 mbar.
- The polycondensation is carried out in the melt phase at a temperature increasing from the entry to the exit of the polycondensation reactor from 252 to 267°C and at an absolute pressure of 0.2 to 2.5 mbar.
- For generating the vacuum of the precondensation and polycondensation vapor-jet pumps are used, which are operated with TMG vapor, and the vapors sucked off and said TMG vapors are compressed by the vapor jet pumps and condensed by spraying them with a liquid which predominantly consists of TMG, for example the condensate from these spray condensers and optionally fresh make-up TMG.

The feed amount of titanium in the first, initial esterification stage preferably is in the range from 5 to 25 ppm.

As catalytic titanium compound to prepare the catalyst liquid there may preferably be used titanium tetrabutylate or titanium tetraisopropylate. As advantageous catalytic titanium compounds there may for instance also be used any catalytic titanium compound, such as titanium alkylates and their derivatives, like tetra-(2-ethylhexyl)-titanate, tetrastearyl titanate, diisopropoxy-bis-(acetyl-acetonato)-titanium, di-n-butoxy-bis-(triethanolaminato)-titanium,

tributyl monoacetyltitanate, triisopropyl monoacetyltitanate or tetrabenzoic acid titanate, titanium complex salts, like alkali titanium oxalates and malonates, potassium hexafluorotitanate, or titanium complexes with hydroxycarboxylic acids such as tartaric acid, citric acid or lactic acid. Also special catalysts as titanium dioxide - silicon dioxide - co-precipitate or hydrated alkaline containing titanium dioxide can be used.

10 The solvent which is used in the liquid catalyst feed is TMG, in which for stabilization reasons a C_4 to C_{12} dicarboxylic acid is dissolved in quantities below its saturation concentration at ambient temperature. A further embodiment consists in that in TMG C_2 to C_{12} monocarboxylic acid is dissolved below its saturation concentration

—
20 The organic di-acid which is preferably used for the liquid catalyst feed is selected from terephthalic acid, isophthalic acid or another C_4 - C_{12} aromatic or aliphatic dicarboxylic acid. Preferably the C_4 to C_{12} dicarboxylic acid is incorporated in the PTT and does not act as chain stopper.

25 As further embodiment of the invention the catalyst liquid can be a Ti containing liquid reaction product from TPA and TMG with a degree of esterification of at least 97%. This product is recycled from a later reactor stage and mixed to the first, initial esterification process together with the raw materials. In the continuous process the recycled product amounts to 5 to 40 wt-%, more preferably to 10 to 30 wt-% of the nominal throughput. In the case of the batch process the amount of recycled product lies between 25 and 85 wt-%, preferably between 35 and 70 wt-% of the nominal batch size. This option of the invention is including reaction products which may be withdrawn at any point 35 between the exit from the second stage of esterification and the entry in the polycondensation, and which are used

as liquid catalyst feed for the first initial esterification stage.

5 The second portion of the catalyst may be fed after the esterification step.

10 An important aspect of the invention consists in that in the initial stage of esterification a specific combination of parameters is used. The described special catalyst liquid is well proven at temperatures within the range of 245 to 260°C, an elevated molar feed ratio of TMG to TPA between 1,5 and 2,4 and a pressure of 1 to 3,5 bar. At this conditions only a minor formation of non-filterable particles occurs independently whether delustering agents, 15 like TiO_2 , or other additives are used. This is particularly necessary in the production of fibers.

— In accordance with a further preferred aspect of the invention, the first initial stage of esterification is 20 conducted to a TPA conversion of 90 to 95%, and the at least second stage of esterification rises the TPA conversion to 97 up to 99%. Latest in the second stage of esterification it has been assured that the last particles of solid TPA from 25 the paste are completely dissolved and the melt is clear and bright.

The catalyst liquid introduced into the second or further stages of esterification is preferably a clear solution. 30 These above mentioned conditions enable low filter values of the PTT.

The process can be a continuous or a batch process. In the discontinuous process the initial process cycle with a 35 transiently heterogeneous reaction mixture and a limited TPA-conversion of below 95% is considered as the first, initial stage of esterification, while the later reaction

cycle in a homogeneous melt phase at a TPA-conversion of at least 97% represents the at least one subsequent esterification stage. Accordingly the second part of the liquid catalyst feed is added when the TPA has been
5 esterified to at least 95%, preferably to more than 97%.

The precondensation, especially in the continuous process, is favourably split into two pressure sections to provide
10 an optimum condensation progress. The first stage of precondensation is performed between 50 and 150 mbar, the second stage between 2 and 10 mbar.

It is particularly advantageous when the polycondensation of the prepolymer melt is performed at a pressure of 0.3 to 0.8 mbar. Preferably the polycondensation reactor is a disc
15 ring reactor or a cage type reactor, which allows the formation of steadily renewed, large film surfaces of the reaction product and facilitates by this the evaporation of the split products. Under these conditions, increased
20 intrinsic viscosities in the range from 0.75 to 1.15 dl/g are possible.

It was surprisingly found out that in accordance with the inventive process very advantageous filter values of 0 to
25 40 bar·cm²/kg can be realized (determination of filter value see below).

In accordance with a further object of the invention it is provided that the condensates of the spray condensers, optionally after the distillation of low boilers, are
30 recirculated into the first initial and possibly further stages of esterification. In this way, a substantial reduction of the losses in raw materials is achieved.

In accordance with a further preferred embodiment of the invention it is provided that the PTT contains up to 20 wt-
35 % comonomer units derived from other dicarboxylic acids and/or diols. As other dicarboxylic acid there may for

instance be used adipic acid, isophthalic acid or naphthalene dicarboxylic acid. As diols there may for instance be used ethylene glycol, diethylene glycol, triethylene glycol, butylene glycol, polyglycols as well as
5 cyclohexane dimethanol. In this way, the end product can be adapted to the respective application relatively easily.

A further embodiment of the invention consists in that at any point before the end of the polycondensation in the
10 melt phase usual additives such as delustering agents and/or color agents and/or branching agents and/or stabilizers can be added. By means of this measure, the number of the applications of the end product will be increased in connection with a particular viscosity
15 adjustment.

In accordance with the invention, a polyester-soluble cobalt compound, for instance cobalt acetate and/ or polyester soluble organic dyes can be used as color agent
20 or blue toner. As stabilizer a phosphorus compound is added with up to 20 ppm phosphorus, based on PTT, in connection with the cobalt compound and up to 10 ppm phosphorus without any addition of cobalt. By this amounts of phosphorus the catalysis of the thermal degradation of the
25 PTT melt by ions of heavy metals including of the cobalt is stopped because of the formation of neutral phosphorus salts. In special cases the addition of phosphorus may be omitted completely; this depends on the quality of the raw materials, the construction materials of the equipment as
30 well as on the final product application.

A further aspect of the invention consists in that optionally carboxylic acids with three or more COOH groups, polyfunctional acid anhydrides, or polyfunctional alcohols
35 with three or more OH groups, or carboxyphosphonic acids or the esters thereof in concentrations below 5000 ppm are used as branching agents. For polycarboxylic acids and

polyalcohols in most cases concentrations below 1000 ppm are sufficient. These compounds can particularly be used for adjusting or raising the intrinsic viscosity simultaneously.

5

The PTT can be directly processed to fibers, films or other molded materials. In accordance with a further embodiment of the invention it is provided that after the polycondensation in the melt phase the PTT is granulated and crystallized.

10

The resulting granulate can also be thermally treated in the solid state for further IV build up or for devolatilizing low molecular organic products such as acrolein, allyl alcohol and water. The PTT granulate can then be processed to fibers, filaments, films or molded articles.

15

The processed products, i.e. fibers, filaments, films, molded articles or chips, are characterized by an IV of 0.8 to 1.1 dl/g, a filterability of $< 40 \text{ bar} \cdot \text{cm}^2/\text{kg}$ and a thermal stability (as defined below) of $> 80\%$.

20

The subject-matter of the invention will be explained in detail with reference to the following examples.

25

In all examples, the intrinsic viscosities (IV) were determined with a solution of 0.5 g polyester in 100 ml of a mixture of phenol and 1,2-dichlorobenzene (3:2 parts by weight) at 25°C.

30

The COOH terminal group concentration was determined by photometric titration with 0.05 n ethanolic potassium hydroxide solution against bromothymol blue of a solution of polyester in a mixture of o-cresol and chloroform (70 : 30 parts by weight).

35

The measurement of the polymer color values was made on crystallized polyester granules (crystallization at $150 \pm 5^\circ\text{C}/1\text{ h}$) in a tristimulus colorimeter containing three photoelectric cells with a red, green or blue filter. The color values were calculated from the parameters X, Y and Z according to CIELAB.

The filtration behavior of the product melts was determined as follows: PTT dried for 13 h at 130°C and a reduced pressure of $< 1\text{ mbar}$ was molten in a laboratory extruder and metered through a disc filter with a mesh size of $15\text{ }\mu\text{m}$ and a filter area of 2.83 cm^2 by means of a gear pump at a temperature of 260°C . The increase in pressure before the filter was recorded in relation to the amount of melt conveyed and the filterability is calculated as filter value (FV):

$$\text{FV} = \text{filter pressure}[\text{bar}] \cdot \text{filter area}[\text{cm}^2] / \text{amount of melt}[\text{kg}]$$

The thermal stability (TS) of the PTT melt was determined by measuring the intrinsic viscosity of the PTT chips dried for 13 h at 130°C and a reduced pressure of $< 1\text{ mbar}$ as IV_0 before and as IV_T after tempering of the dried chips over one hour at a reference temperature of 255°C in a closed tube under nitrogen.

$$\text{TS} [\%] = 100 \cdot IV_T / IV_0$$

The stated concentrations of the catalysts and additives used in the following examples are defined as parts per million (ppm) referring to the TPA feed.

The catalyst solutions used in the examples according to the invention were prepared as follows:

Catalyst preparation A:
(TPA-stabilized TMG solution)

Because of the hygroscopic properties of TMG, the catalyst solutions were preferably prepared and stored under nitrogen atmosphere.

5

TMG was preheated to 80°C. 50 mg TPA per kg TMG were added while stirring, and stirring was continued until a clear solution was obtained after 20 minutes. The TMG/TPA solution was cooled to about 30 °C.

10

The titanium tetrabutylate was metered with a dropping funnel to the cold, clear acidified TMG solution while stirring. There was thus produced a solution of 2% titanium tetrabutylate in acidified TMG, which was used in this form. When the first drops of titanium tetrabutylate were added, the TMG solution turned light yellow. Remarkably, this color did not change anymore during the further addition of titanium tetrabutylate.

15

20

Catalyst preparation B:
(IPA-stabilized TMG solution)

25

The TMG was preheated to about 60°C. Then a clear solution of 500 mg IPA per kg TMG was produced by stirring. This concentrated solution was cooled to about 30°C. Before adding the titanium tetrabutylate the cooled solution was diluted with fresh TMG in a ratio of 1:4. Thus, the concentration of IPA in the finished solution was 100 mg IPA per kg TMG.

30

The addition of the titanium tetrabutylate to the TMG/ IPA solution was performed in the same way as for preparation A.

35

The invention is illustrated in the following examples.

The results of the examples are summarized together with the fed concentrations of catalyst and additives in the table. examples 1, 2 and 4 are comparative examples.

5 Example 1-3 (Batch process)

10 In this batchwise production of PTT a part of prepolymer from a preceding, prepolymer batch in a quantity of about 42 wt-% of the nominal batch size was kept back in the esterification reactor for the next reaction cycle for stirring the esterification product and for feeding and heating the raw materials TMG and TPA as a paste including the esterification catalyst and optionally cobalt acetate as color agent. The molar TMG to TPA feed ratio of the
15 paste is listed in the table.

— The quantity of TPA fed into the esterification reactor was 180 kg. The feeding time was 130 minutes. The total cycle time of esterification in example 1-2 was 160 minutes at a
20 temperature of 265°C and a pressure of 1000 mbar (abs.). A column disposed subsequent to the esterification reactor was used for separating the low-boiling compounds, mainly process water, from the trimethylene glycol in the vapors from the esterification, and for the recirculation of the
25 distilled TMG to the process all the time of esterification. The precondensation was carried out in 30 minutes at a simultaneous pressure reduction to 50 mbar (abs.). Thereafter, the prepolymer melt was transferred to a disc ring reactor, and the polycondensation was started
30 by agitating defined by a standard program of speed control and further reducing the pressure within 45 minutes to 0.5 mbar as final pressure. The polycondensation temperature in example 1-2 increased from 260 to 268°C. The total duration of polycondensation indicated in the table
35 corresponded to the maximum viscosity of the polymer possible under the selected conditions, i.e. if the polycondensation was further continued, the intrinsic

viscosity of the polymer decreased again due to the predominance of the thermal degradation reactions. Upon reaching the viscosity maximum, the polycondensation was stopped. At an applied pressure of 55 to 60 bar the polymer melt was discharged from the reactor and granulated.

Special feed conditions within example 1 (comparative)

In example 1, titanium dioxide/silicon dioxide co-precipitate containing 80 mole-% TiO_2 with 50 ppm Ti was fed to the paste as esterification catalyst. In addition, cobalt acetate with 40 ppm Co was added to the paste. Before starting of the precondensation, phosphoric acid with 40 ppm P was added to the melt and after further 2 minutes antimony triacetate with 250 ppm Sb was added as polycondensation catalyst.

Special feed conditions within example 2 (comparative)

In example 2, titanium tetrabutylate with 75 ppm Ti was fed to the paste as esterification catalyst. Before start of the precondensation reaction in the esterification reactor, antimony triacetate with 200 ppm Sb was added as polycondensation catalyst.

Selected process conditions and quality values of the polytrimethylene terephthalate obtained are listed in the following table. In the comparative process very high amounts of catalyst up to 300 ppm were required. In the following inventive examples 80 ppm Ti were sufficient at comparable process times. The process results of the Comparative examples show a deficit with regard to the possible IV- build-up, the thermostability and the filterability.

Special conditions within example 3 (inventive)



According to example 3, TMG and commercially available TPA in a molar ratio of 1.3 were continuously fed into a paste mixer; additionally 15 ppm titanium were added via a catalyst liquid of titanium tetrabutylate in TMG containing TPA according to catalyst preparation A. The resulting paste was fed into the esterification reactor over 130 minutes and reacted batchwise (similar to example 1 and 2). The reaction was performed at an increased pressure of 2000 mbar and at a temperature of 255°C during a cycle time of 160 minutes. The column of the esterification was operated at a molar recycling ratio of TMG to TPA of 0.1 to 0.9, which ratio passed through a maximum during the esterification time. The average total molar feed ratio of TMG to TPA in the esterification reactor was about 1.8.

For completion of the esterification, the reactor pressure was reduced to 1000 mbar within 15 minutes and the esterification was continued in the later stage while stirring at 1000 mbar for 30 minutes. At 5 minutes before starting the vacuum program 65 ppm titanium were added to the esterification product as polycondensation catalyst via the catalyst liquid of preparation A at steady stirring of the product mixture. The subsequent precondensation was carried out during 30 minutes at a temperature of 255 °C and a simultaneous reduction of the pressure to 100 mbar. Subsequently, the melt was transferred to a disc ring reactor, where it was polycondensated at an increasing temperature of 251 - 262°C at a dwell time of 165 minutes and a final pressure of 0.5 mbar. Thereafter the melt was discharged and granulated to PTT chips.

This example clearly illustrates according to the table that under batch conditions, when using the conditions described in the present invention, a stable PTT with an IV of 1:1 dl/g and a filter value of 27 bar·cm²/kg can be produced. The relatively low concentration of carboxyl endgroups in the PTT indicated that no remarkable polymer

degradation during discharge of the PTT occurred. The thermal stability of the PTT enabled a problem-free extrusion and spinning or molding to obtain high quality PTT products.

5

Example 4 to 8(continuous process)

Example 4 (comparative)

10 TMG and commercially available TPA in a molar ratio of 1.16 were continuously fed to a paste mixer, and a paste was produced. The catalyst concentration in the paste was 15 ppm titanium. As catalyst titanium tetrabutylate was used as a

15 10% mixture with TMG. The paste was continuously fed into the initial esterification reactor and reacted at a pressure of 1000 mbar and a temperature of 255°C for a mean dwell time of 172 minutes under stirring and steady TMG reflux from the esterification column. Into the transfer

20 line to a subsequent stirred esterification stage, a second portion of the catalyst (10% titanium tetrabutylate in TMG) with 65 ppm Ti was added, and the product was further esterified in the subsequent esterification stage at a pressure of 1000 mbar, a temperature of 255°C with a mean

25 dwell time of 60 minutes. The esterification product was transferred into a third reaction stage also equipped with a stirrer for precondensation at 100 mbar and 255 °C within 30 minutes.

30 Likewise the precondensation was completed in a further stage at 7 mbar, 257°C within 35 minutes. The precondensate, showing an IV of 0.26 dl/g was transferred to a disc ring reactor by means of a gear-type metering pump for the final polycondensation at a vacuum of 0.5

35 mbar, a mean dwell time of 150 minutes, an increasing temperature profile of

258-264°C and an agitator speed of 5.5 rpm. From the disc ring reactor, the melt was discharged and granulated.

5 The PTT thus produced had an intrinsic viscosity of 0.92 dl/g and a filter value of 143 bar·cm²/kg. The higher concentration of carboxyl endgroups in the PTT indicated another, from the invention different polymer formation, whereas the thermal properties of the products were similar. Polymers with such high filter values entail to a short service life of the filter in the spinning process, and are not suitable for the production of fibers and filaments.

Example 5

15 In example 5, the conditions for the production of PTT corresponded to example 4 with following exceptions. The molar ratio TMG:TPA in the paste was risen to 1.3; the catalyst concentration in the paste was 15 ppm titanium. As catalyst liquid the catalyst preparation B was used. The paste was continuously fed into the first initial esterification reactor and reacted while stirring at a pressure of 2000 mbar and a temperature of 255°C for a mean dwell time of 172 minutes. The molar reflux from the column of the esterification amounted to 0.8 moles TMG per TPA; by this a total molar ratio of TMG to TPA of 2.1 was present. After the continuous transfer to a second subsequent esterification stage, a further amount of catalyst of 65 ppm Ti was added into the mixed esterification product in form of the catalyst preparation B. The esterification in the second stage, the precondensation and the polycondensation were performed at conditions identical to those in example 4.

35 The PTT thus produced had an intrinsic viscosity of 0.93 dl/g and a filter value of 5 bar·cm²/kg. The good filter value of the intermediate prepolymer sample of 8



100

bar·cm²/kg, already indicated a good filterability of the melt. In the PTT production process and in the production of fibers and filaments this offers great economic advantages due to a long service life of the filter.

Example 6

Similar to example 5, TMG and TPA were continuously fed into the paste mixer in a molar ratio of 1.25. Thereby 70 wt-% of the TMG used consisted of recycled TMG collected from the vapor condensers of different stages. The concentration of solids (a mixture of PTT oligomers) in the recycled TMG was 2.5 wt-%. In addition, 15 ppm titanium as catalyst solution, preparation B, and 20 ppm Co as cobalt acetate were added to the raw material paste, and the paste was pumped to the initial esterification stage. The total molar TMG to TPA feed ratio including the TMG- reflux from the column was 1.9. All other process conditions in esterification, precondensation and polycondensation were selected in accordance with example 4. According to example 5, additional 65 ppm Ti were added into the mixed esterification product of the subsequent second esterification stage. As catalyst liquid feed was used preparation B. Additionally 20 ppm P (as solution of phosphoric acid in TMG) were dosed into the transfer line of the esterification product to the first precondensation stage.

The granulated PTT had a viscosity of 0.918 dl/g and a filter value of 7 bar·cm²/kg.

Example 7:

Example 7 was performed in a similar way as example 6, and for the production of paste there was likewise used recycled TMG. The molar ratio TMG to TPA was 1.25. 46 wt-%

of the TMG present in the feed paste were recycled TMG with a content of oligomeric solids of 2.2 wt-%. Different to example 6, 10 ppm Co as cobalt acetate and 5 ppm P as phosphoric acid were added to the paste. The catalyst feed into the paste was 15 ppm Ti as catalyst liquid preparation A. The polycondensation catalyst was added in an amount of 65 ppm Ti, as catalyst liquid preparation A to the melt of the subsequent second esterification stage. The other process conditions were as following:

Total TMG/TPA - mol ratio= 1.9

1 st	Esterification stage:	249°C	2000 mbar	230 min
2 nd	Esterification stage:	248°C	1000 mbar	30 min
1 st	Prepolycond. stage:	247°C	80 mbar	37 min
2 nd	Prepolycond. stage:	247°C	8 mbar	41 min
	Polycondensation stage:	247-260°C	0.3 mbar	220 min

Under these process conditions a PTT was obtained with an IV of 0.93 dl/g, a high thermal stability and a good filterability.

Example 8

(Continuous process with recirculation of the melt from esterification 2 to esterification 1)

TMG and TPA were continuously fed into the paste mixer in a molar ratio of 1.25. Thereby, 58 wt-% of the TMG used consisted of recycled TMG with 2 wt-% of oligomeric solids. After achieving stationary flow conditions the TMG/TPA feed paste without any catalyst was transferred to the first, initial stirred esterification stage. At the same time a separate partial recycling stream of 19 wt-% of the product from the subsequent second esterification stage to the first initial stage containing the catalyst as a diluted

solution in a prereacted homogenous product mixture with an increased degree of esterification of about 97,5%.

5 The actual catalyst addition to the second esterification stage was carried out with 80 ppm Ti (based on PTT) as liquid catalyst preparation B. As a consequence of the partial product recycling from the second subsequent esterification stage into the initial esterification stage the relative throughput per 100 wt-% product was in both
10 esterification stages increased to 119 wt-% and the average residence times were decreased to 135 and 48 minutes. The total molar TMG to TPA feed ratio to the esterification was 2.0. Further conditions were:
15 1st esterification stage: 255°C 1800 mbar
2nd esterification stage: 255°C 1000 mbar.

— The process conditions in the precondensation and polycondensation were the same as in example 4. The final
20 PTT product showed an IV of 0.913 dl/g, a good thermal stability, and a good filterability, in accordance with the invention.

Claims:

1. A process of producing polytrimethylene terephthalate (PTT) with an intrinsic viscosity of at least 0.75 dl/g by
5 esterification of terephthalic acid (TPA) with tri-
methylene glycol (TMG) in the presence of a catalytic
titanium compound to obtain an esterification product,
precondensation of the esterification product to obtain a
10 precondensation product and polycondensation of the
precondensation product to obtain PTT, characterized in
that

a) the esterification is performed in at least two stages,
15 a first, initial stage and at least one second, subsequent
stage connected to a process column,

b) a liquid catalyst feed is prepared on base of TMG
having a concentration of less than 5 wt-% titanium in the
20 form of a titanium compound stabilized by a bifunctional
organic acid,

c) a major quantity between 65 and 100% of said liquid
catalyst feed containing 35 to 110 ppm titanium, is
25 introduced into the at least one subsequent esterifi-
cation stage, operated at a temperature of 245 to 260°C,
and a pressure of 0.7 to 1.2 bar,

d) a minor quantity of said liquid catalyst feed
30 containing 0 to 40 ppm titanium and equal in maximum to 35%
of the total catalyst is directly fed to the initial
esterification stage usually together with the raw
materials, which direct catalyst feed can be partially or
completely substituted by the same quantity of catalyst in
a reaction product, which may be recycled from any further
35 reaction stages and which is mixed to the raw materials for
further reaction in said initial esterification stage in
connection with a total molar TMG to TPA feed ratio of 1.15



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to 2.5, a temperature of 240 to 270 °C and a pressure of 1 - 3.5 bar,

5 e) the precondensation is performed at a temperature of 245 to 260°C under a reduced pressure between 2 and 200 mbar,

10 f) the polycondensation is carried out in the melt phase at a pressure of 0.2 to 2.5 mbar, a temperature of 252 to 267°C, basically increasing from the entry to the exit of the polycondensation reactor during agitation and formation of steadily renewed, large film surfaces of the reaction product for evaporation of the split products, and

15 g) for generating the vacuum to perform the precondensation and polycondensation vapor-jet pumps are used to remove the released TMG and PTT oligomers and low boilers from the gas phase of the reactors, and the vapor-jet pumps are operated with TMG vapor, and the vapors
20 sucked off and compressed by the vapor-jet pumps and said TMG vapors are condensed by spraying them with a liquid which predominantly consists of TMG.

25 2. A process as claimed in claim 1, characterized in that said titanium compound is a titanium alkylate, like titanium tetrabutylate, titanium tetraisopropylate or tetra-(2-ethylhexyl)-titanate, or a titanium dioxide - silicon dioxide - co-precipitate or a hydrated sodium containing titanium dioxide or a titanium salt of organic
30 acids or a titanium complex with hydroxycarboxylic acids.

35 3. A process as claimed in any of claims 1 to 2, characterized in that said liquid catalyst feed contains trimethylene glycol, in which a C₄ to C₁₂ dicarboxylic acid is dissolved below its saturation concentration.

4. The process as claimed in claim 3, characterized in that terephthalic acid or isophthalic acid is used as C_4 to C_{12} dicarboxylic acid.
- 5 5. The process as claimed in any of claims 1 to 2 characterized in that said liquid catalyst feed contains tri-methyleneglycol, in which a C_2 to C_{12} monocarboxylic acid is dissolved below its saturation concentration.
- 10 6. A process as claimed in any of claims 1 to 5, characterized in that the process is a continuous process.
- 15 7. A process as claimed in claim 6, characterized in that a part of the reaction product is withdrawn at any point between the exit of the subsequent stage of esterification and the entry to the polycondensation and mixed to the raw materials by recycling said reaction product to the first, initial esterification stage.
- 20 8. A process as claimed in claim 7, characterized in that said reaction product recycled to the initial esterification stage lies in the range of 5 to 40 wt-% of the nominal throughput.
- 25 9. A process as claimed in any of claims 1 to 5, characterized in that the process is a discontinuous process, and the initial process cycle with a transiently heterogeneous reaction mixture and a limited TPA-conversion of below 95% represents said 'initial stage' and the later
- 30 reaction cycle in a homogeneous melt phase with a TPA conversion of at least 97% represents said 'subsequent stage' of the esterification process, to which the major part of the catalyst is fed, and a portion of the reaction product kept back at the end of the precondensation is used
- 35 for the next discontinuous process in step d as catalyst containing reaction product.

10. A process as claimed in any of claims 1 to 9 characterized in that the second portion of the catalyst is fed after the esterification step.
- 5 11. A Process as claimed in claim 9, characterized in that said catalyst containing reaction product recycled to the initial esterification stage lies in a range of 25 to 85 wt-% of the nominal batch size.
- 10 12. A process as claimed in any of claims 1 to 11, characterized in that the first, initial stage of esterification is conducted to a degree of esterification of 90 to 95%, and the subsequent stage of esterification is conducted to a degree of esterification of 97 to 99%.
- 15 13. A process as claimed in any of claims 1 to 12, characterized in that the condensed vapors from step g are recirculated to the initial and possibly further subsequent stages of the esterification, optionally after removing of the low boilers from TMG by distillation.
- 20 14. A process as claimed in any of claims 1 to 13, characterized in that the PTT contains up to 20 wt-% comonomer units derived from other dicarboxylic acids and/or diols.
- 25 15. A process as claimed in any of claims 1 to 14, characterized in that at any point before the end of the polycondensation in the melt phase usual additives such as delustering agents and/or color agents and/or branching agents and/or stabilizers are added.
- 30 16. A Process as claimed in any of claims 1 to 15, characterized in that said polycondensation reactor is a discing reactor or a cage type reactor.
- 35

17. A process as claimed in any of claims 1 to 16,
characterized in that the PTT is after the polycondensation
in the melt phase granulated to chips, and the chips are
5 dried, crystallized and treated thermally in the solid
phase.

18. A process as claimed in any of claims 1 to 17,
characterized in that the PTT is processed to products,
10 like fibers or filaments or films or molded articles or
chips.

19. A process as claimed in claims 18, characterized in
that the processed products have an IV of 0.8 to 1.1 dl/g,
15 a filterability of $< 40 \text{ bar} \cdot \text{cm}^2/\text{kg}$ and a thermal stability
(as defined before) of $> 80\%$.

Abstract:

Process of producing polytrimethylene terephthalate (PTT) by esterification of terephthalic acid (TPA) with trimethylene glycol (TMG) in the presence of a catalytic titanium compound, precondensation and polycondensation. The esterification is effected in at least two stages, where in the first stage a molar ratio of TMG to TPA of 1.25 to 2.5, a content of titanium of 0 to 40 ppm, a temperature of 245 to 260°C as well as a pressure of 1 to 3.5 bar are adjusted. In the at least one subsequent stage a content of titanium is adjusted which is higher than in the initial stage by 35 to 110 ppm. For generating the vacuum in the polycondensation and in the precondensation, there are used vapor jet pumps operated with TMG vapour.

